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AEROMETRICS

DEVICE FOR MEASURING THE
TEMPERATURE OF LIQUID AND GASEOUS HYDROGEN

CONTRACT NAS8-11862

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APRIL 1966

NASA - MARSHALL SPACE
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AEROMETRICS
AEROJET-GENERAL CORPORATION
San Ramon, California

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April 1966

NASA - MARSHALL SPACE FLIGHT CENTER
Huntsville, Alabama

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I. INTRODUCTION

This report is prepared to fulfill the requirements of Contract NAS8-11862, for the design, development and fabrication of a device to measure the temperature of liquid and gaseous hydrogen.

Contract NAS8-11682 provided for the development of a wide range (-253°C to +60°C) temperature transducer for measurement of liquid and gaseous hydrogen. Three pre-production prototype transducers were fabricated, tested and delivered in February, 1966. Thirteen production transducers were fabricated, tested and delivered in March 1966.

Aerometrics' Proposal LR 651604 delineated the program which was followed to develop this wide range transducer.

The objective of the program was to develop a temperature sensor to meet the following requirements:

- | | |
|-------------------------|---|
| (1) Range: | -253°C to +60°C. |
| (2) Pressure: | 40 psia maximum. |
| (3) Output: | 5 vdc when amplified with a gain of 100. |
| (4) Interchangeability: | ±1% for range -253°C to 60°C. |
| (5) Repeatability: | ±0.1°C (-253°C to -190°C).
±0.2°C (-190°C to +60°C). |
| (6) Response: | Less than 100 milliseconds for 63.2% of the temperature change when the sensor is moved from under the surface of liquid hydrogen to a static hydrogen ullage at a temperature of -190°C. |

All details of this contract are reported including the test data.

II. SUMMARY AND CONCLUSIONS

This development program has resulted in producing a cryogenic temperature transducer which is extremely fast in response to changing temperatures, medium accuracy and measures temperature over a wide range.

The transducer will respond to a temperature change from -246°C to -196°C in 0.1 seconds (63% or 1 time constant). An accuracy of 0.3°C is typical over the -253°C to -190°C span when cycled between ambient and cryogenic temperatures repeatedly. The range of the transducer is designed for -253°C to 60°C .

The most unusual characteristic of the transducer is the shaped output curve. This curve is shaped to have a very high sensitivity in the liquid hydrogen range and low sensitivity over the remaining temperature span. Typical sensitivity at liquid hydrogen is $1.35 \text{ mv}/^{\circ}\text{C}$. The output signal is also adequate for most recording systems, typically 20 mv at $+60^{\circ}\text{C}$ and 60 mv at -253°C .

III. DISCUSSION

A. PRINCIPLE OF OPERATION

The transducer and suggested electrical circuit are as shown in Figure 1. The output signal from the transducers is generated as a result of two transduction modes.

1. The voltage generated by passing a constant current through the temperature dependent resistor. Typical normalized resistance for a 100 ohm, $\pm 5\%$, 1/8 watt Allen Bradley resistor is illustrated in Figures 2 and 3.

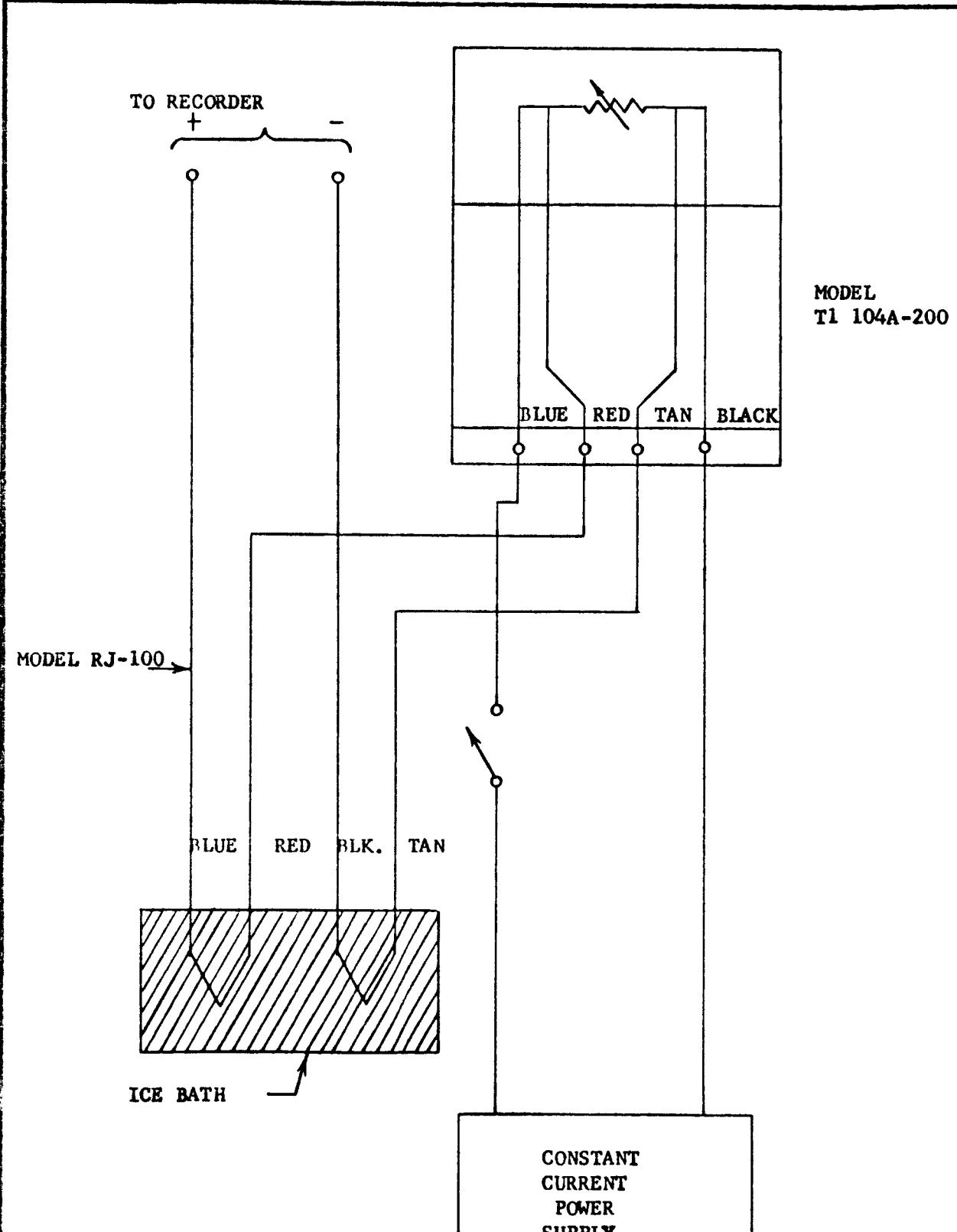
2. The voltage is generated by the thermocouple junction. The magnitude of this voltage is dependent upon the reference temperature and the temperature of the junction.

The two voltages are combined in the transducer to have a single output voltage which varies with temperature. Figures 4 and 5 illustrate the magnitude of these signals and the combined output curve for one of the delivered production transducers. For the -253°C to -190°C range, the transducer output varies exponentially with temperature and for the -190°C to $+60^{\circ}\text{C}$ range it is nearly linear. The exact output signal between -253°C and $+60^{\circ}\text{C}$ is a function of the constant current. All of the calibration data are based upon a 0.23 milliamp current which provides an average signal of 41.437 mv (no load) and 41.317 mv (with 100K load) for all 13 production transducers.

A summary of the output signal of the 13 production transducers is shown in Table 1.

Table 1

SN	OUTPUT - MILLIVOLTS							
	60°C		0°C		-190°C		-253°C	
No Load	100K Load	No Load	100K Load	No Load	100K Load	No Load	100K Load	No Load
2	18.703	18.675	22.453	22.438	35.907	35.855	60.083	59.928
4	19.735	19.703	23.112	23.092	36.882	36.826	62.269	61.836
5	18.413	18.389	22.344	22.324	35.475	35.422	59.292	59.160
6	19.075	19.067	22.620	22.606	36.102	36.045	60.488	60.340
9	18.830	18.801	22.380	22.352	36.024	35.966	60.076	59.934
10	18.871	18.813	22.294	22.266	35.885	35.832	60.547	60.455
11	18.595	18.570	21.935	21.909	35.387	35.341	59.282	59.141
12	18.882	18.661	22.380	22.350	35.963	35.918	59.950	59.806
19	18.730	18.709	22.280	22.253	35.860	35.807	59.705	59.566
22	19.162	19.139	22.717	22.689	36.771	36.716	61.364	61.210
23	18.756	18.727	22.665	22.635	36.372	36.337	60.646	60.497
24	19.000	18.971	22.533	22.507	36.166	36.113	60.602	60.460
25	19.103	19.075	22.799	22.759	35.921	35.866	60.228	60.085
Av.	18.912	18.869	22.501	22.475	36.055	36.003	60.349	60.186



NOTE: Adjust the constant current power supply

FIGURE - 1 OPERATIONAL CIRCUIT

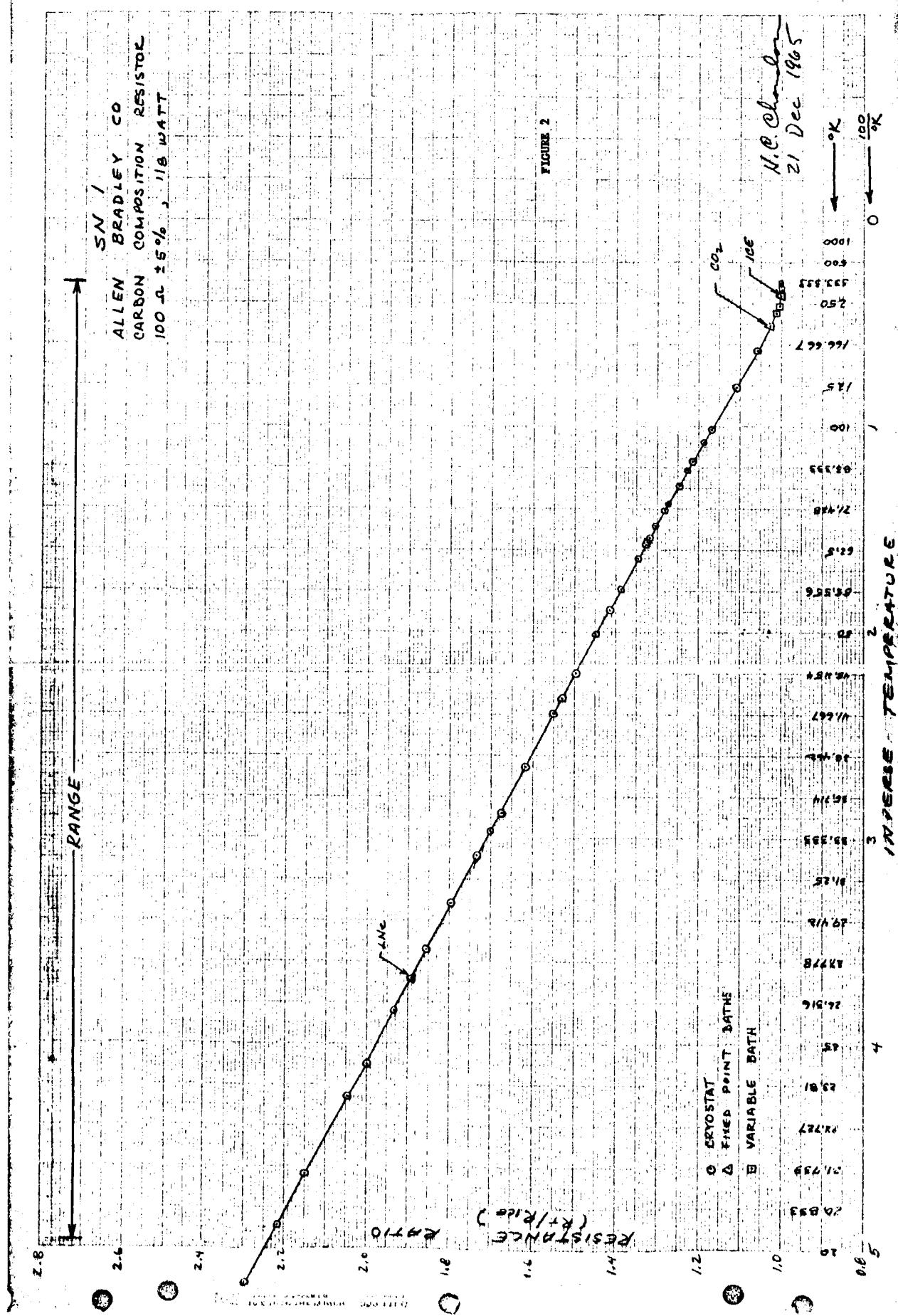
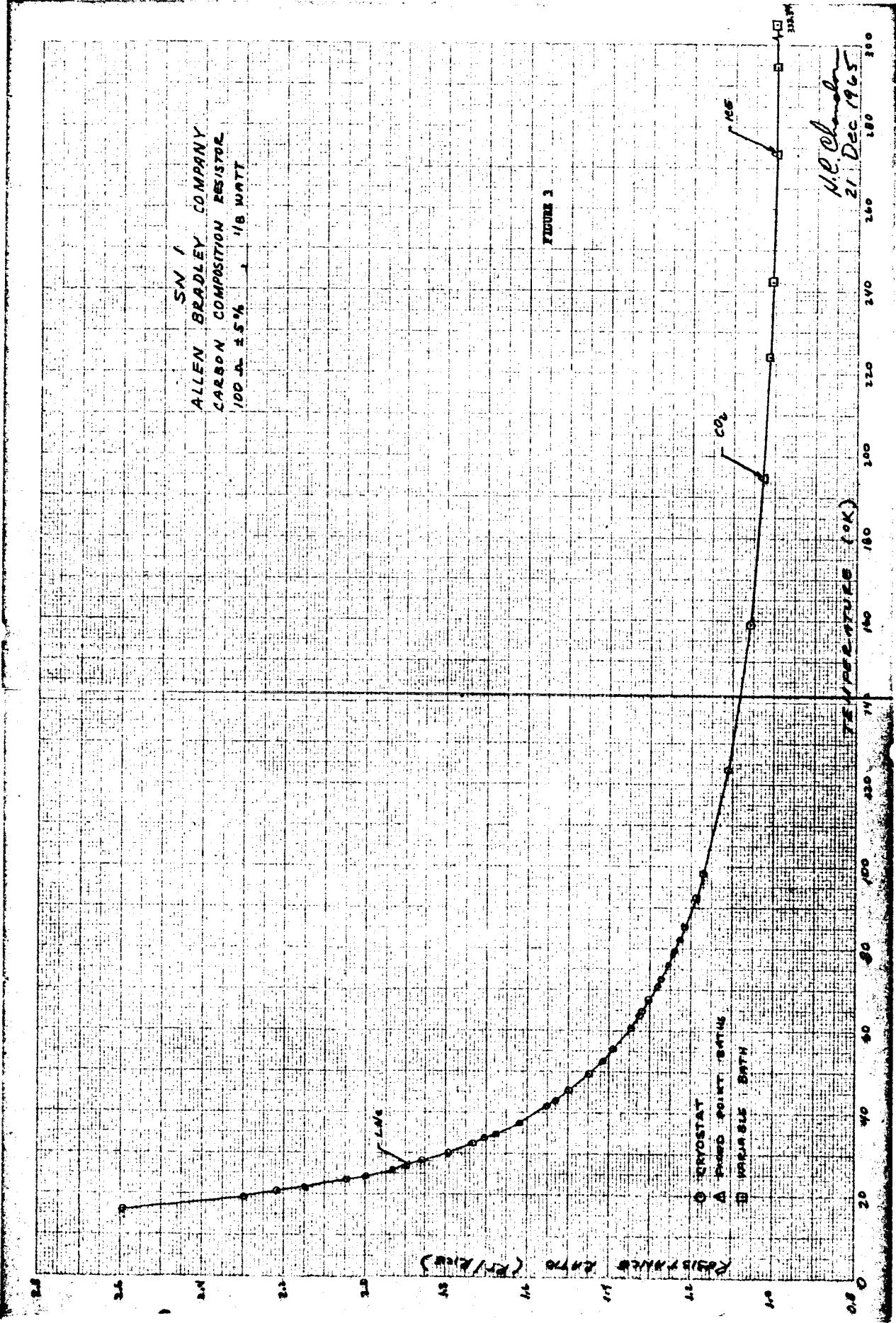
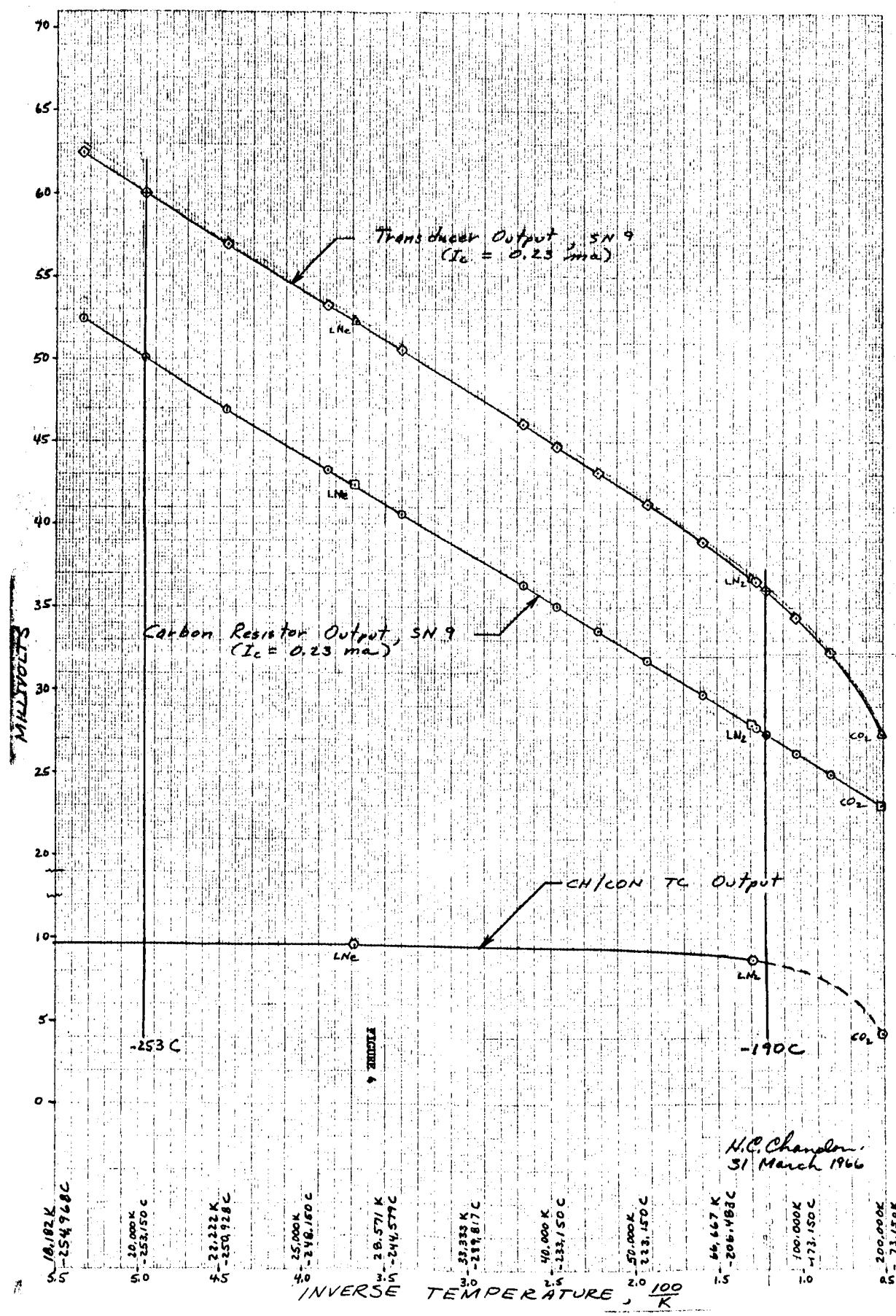
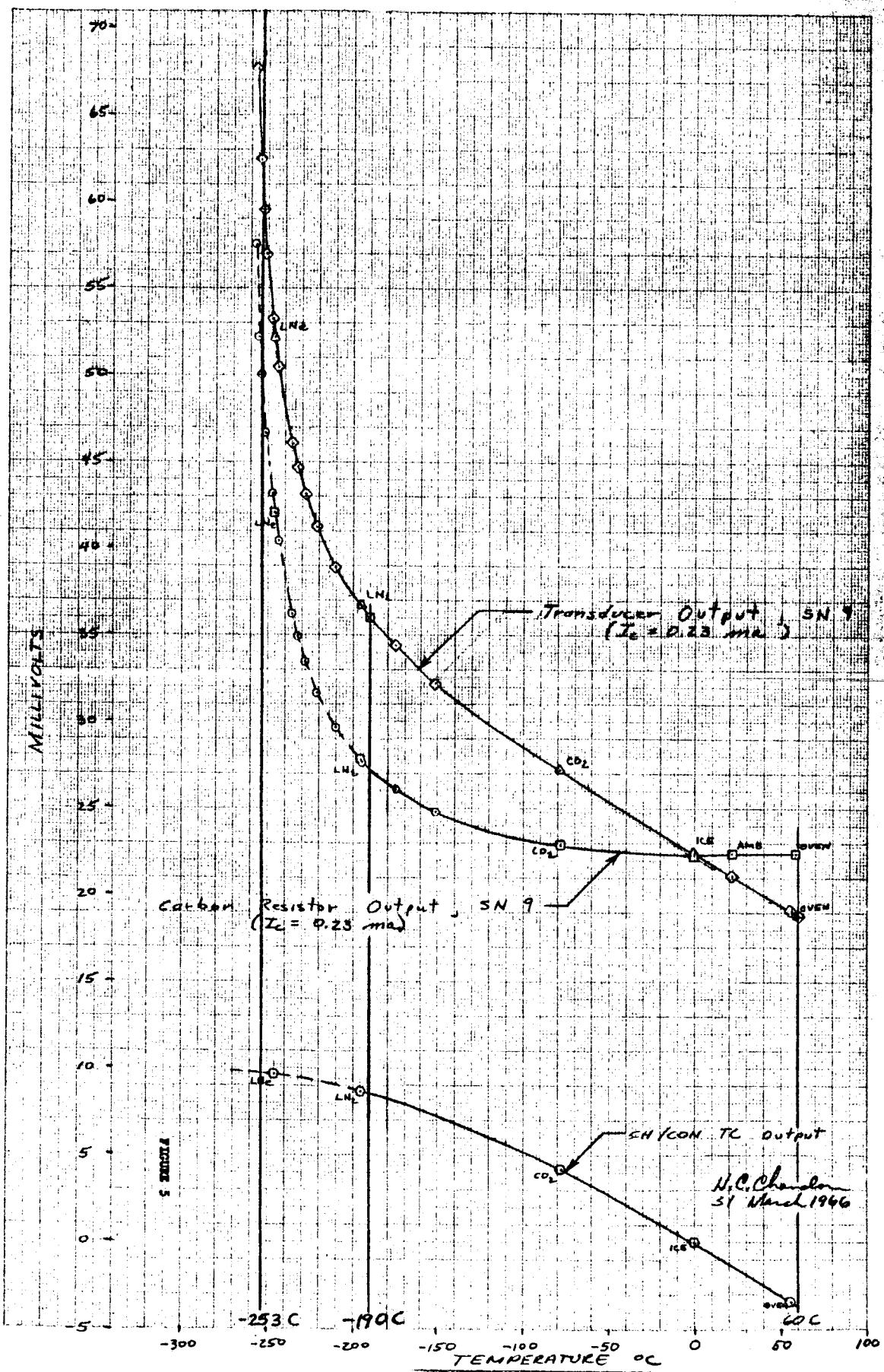


FIGURE 2







As shown, the output is lower than the desired 50 millivolts, for the full span. This is caused by selecting a value for the constant current supply lower than the value required to give a 50 millivolt signal.

The resultant output curve is therefore shaped to provide higher sensitivity at cryogenic temperatures and moderate sensitivity at ambient. Typical sensitivities for SN2 are:

- 0.132 mv/ $^{\circ}$ C (average over the -253 $^{\circ}$ C to +60 $^{\circ}$ C range).
- 1.35 mv/ $^{\circ}$ C at -253 $^{\circ}$ C.
- 1.12 mv/ $^{\circ}$ C at -246 $^{\circ}$ C. (LNE)
- 0.130 mv/ $^{\circ}$ C at -190 $^{\circ}$ C.
- 0.0556 mv/ $^{\circ}$ C at -78 $^{\circ}$ C.
- 0.00927 mv/ $^{\circ}$ C at 60 $^{\circ}$ C.

B. DEVELOPMENTAL PHASE

During the developmental phase of the contract, the following listed items were investigated.

- (1) Element selection.
- (2) Element sealing.
- (3) Transducer design.
- (4) Calibration methods.
- (5) Response test evaluation.

A brief review of each of these phases follows:

1. Element Selection.

Initial testing for stability of carbon resistors from the following companies was achieved during the developmental phase of the program.

<u>MANUFACTURER</u>	<u>MODEL</u>	<u>ASSIGNED SERIAL NUMBER</u>	<u>ELEMENT TYPE</u>
Allen-Bradley	TR	2 thru 9	100 ohm \pm 10%, 1/10 watt carbon composition
Allen-Bradley	EB	1 and 2	91 ohm, \pm 5%, 1/2 watt carbon composition
Allen-Bradley	GB	1 and 2	120 ohm, \pm 5%, 1 watt carbon composition

<u>MANUFACTURER</u>	<u>MODEL</u>	<u>ASSIGNED SERIAL NUMBER</u>	<u>ELEMENT TYPE</u>
Aerovox	RN 20X 60 ROF CPSX-1/2	1 and 2	60 ohm \pm 1%, 1/2 watt
Aerovox	RN 20X 3300%	1	330 ohm, metal film
Speer		1	100 ohm \pm 20%, watt carbon composition

These tests were conducted on randomly selected resistors from the Engineering Laboratory developmental supply.

Allen-Bradley resistors exhibited stability problems at the ice point when cycled between the ice point and liquid nitrogen. Repeated tests did not show a tendency of this shift to decrease in slope or to stabilize. The Aerovox resistors were stable at the ice point, however, they exhibit a very small change in resistance with corresponding change in temperature. For example, the resistance change for the Aerovox units was only 5.5% between ice and LN₂ as compared with 27% for the Allen Bradley resistors. Testing of the less sensitive Aerovox resistors was discontinued in favor of the Allen-Bradley resistors.

2. Element Sealing

During the development of a cryogenic to ambient temperature measuring device, it became necessary to find a carbon resistor of the Allen Bradley 1/8 watt variety which evidenced a stable resistance value at the ice point when cycled between the ice point and liquid helium temperatures. All resistors tested showed a random drift pattern which seemed to indicate moisture absorption. To stabilize this resistor to an ice point resistance accuracy of 0.01%, the following state-of-the-art modification was performed on the resistor.

First, remove all paint and varnish from the resistor to be modified. This may be accomplished by scraping with a sharp tool. Next, apply General Electric Co. Glyptol #7031 resin as thin as possible to the resistor, being careful to cover completely. The resistor is then placed in an atmosphere oven and cured at 50 psig pressure for two (2) hours at ambient temperature ($72^{\circ}\text{F} \pm 5^{\circ}\text{F}$). The resistor is then dried at 100°F for a minimum of 24 hours. If the resistor is then mounted in its

permanent configuration, it will exhibit a stability of $\pm 0.01\%$ at the ice point when cycled between the ice point and cryogenic temperatures.

The 100 ohm $\pm 5\%$ 1/8 watt Allen Bradley resistors have demonstrated the best repeatability at ice point, typically 0.01%, when cycled between LN₂ and ambient.

3. Transducer Design

a. The transducer can be used as a totally immersed type, or for external use with the sensor protruding into the liquid through a boss. When used totally immersed, a jam nut is provided to allow mounting to a flat plate. For use through a boss, the jam nut is removed and an "O" ring installed for sealing.

b. The transducer housing, jam nut, stem and insert are made from type 321 stainless steel. (Figure 6)

c. A special teflon insulated four conductor cable is required for the transducer. The cable is composed of four conductors each of which is made up of five (5) strands of #26 AWG wire to form a #19 AWG conductor. There are two copper conductors, which provide excitation current to the resistor, one chromel thermocouple conductor and one constantan thermocouple conductor. Each conductor is reduced to one #26 AWG wire to allow direct mounting of the resistor to the wires in the stem of the transducer. Figure 7.

d. The element is a sealed and calibrated 1/8 watt Allen Bradley carbon resistor mounted to provide a fast response in hydrogen. Figure 8.

e. The lead wires are secured in the housing by a cryogenically compatible potting compound. (Figure 9)

f. To allow hydrogen flow around the element, the stem is perforated in a pattern which allows easy exit of generated gases and causing a pumping action on the liquid. This stem is required to provide mechanical protection for the element, and as a coupling means for attachment of the transfer tube used for response testing. (Figures 10 and 11)

4. Calibration Methods

Methods had to be developed for calibrating the resistors and completed transducers. They are briefly as follows:

(a) The element must always be protected against direct immersion in water. It was found that direct immersion in water induces thermal EMFS in the circuit which are both large (typically 50 to 100 microvolts) and unstable. This EMF was eliminated by inserting pyrex tubes partially filled with ethanol in the ice baths.

(b) A pyrex tube was also used for element calibrations at CO₂ temperatures, these tubes were placed in the CO₂ test setup and allowed to stabilize before each calibration.

(c) Group calibration of resistor elements when made on 5 elements grouped together per Figure 12. These resistors were then placed inside of the helium-cooled cryostol for multipoint calibration.

5. Response Testing

Experimentation was conducted to define response characteristics for both the element and completed transducers. This data is reported in Section C. The final method selected for testing of the production transducer obtaining temperature step from -190°C to -253°C is as follows:

(a) -190°C to -253°C pre-cool the unit in LN₂ and quickly dunk it in LNe. The corresponding temperatures are -196°C and -246°C.

(b) -253°C to -190°C remove the liquid from around the element. This is accomplished by placing the element inside a tygon tube and blowing the LNe from around the element with GHe. Figures 13 and 14 illustrate the test method.

C. PRE-PRODUCTION PROTOTYPE TRANSDUCERS

1. Introduction

Five pre-production prototype transducers were fabricated and completed. Of these, three were selected for delivery to NASA to fulfill contractual requirements. These units were fabricated in accordance with the production transducer drawings, see Section III-D, except for the following items:

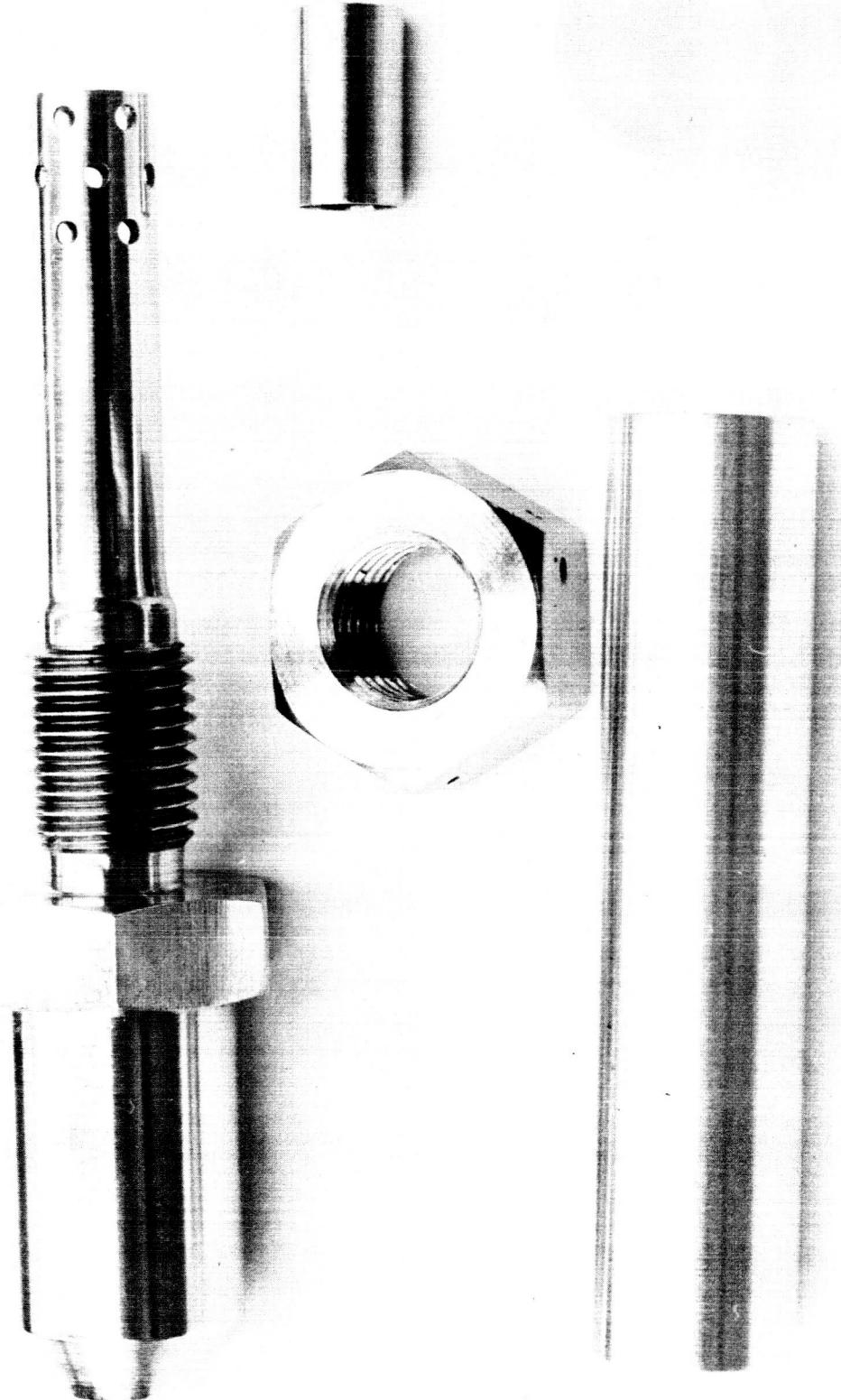


FIGURE 6 - MODEL TI-104A-200 COMPONENT PARTS

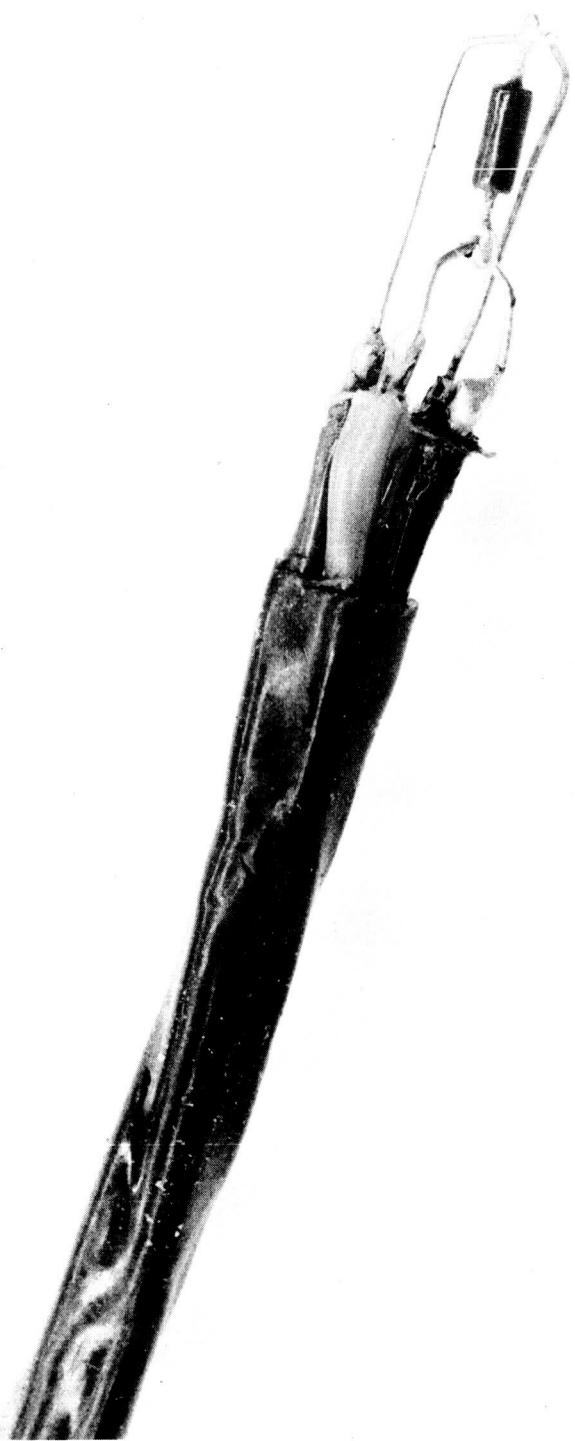


FIGURE 7 - MODEL TI-104A-200 LEADWIRES WITH MOUNTED ELEMENT

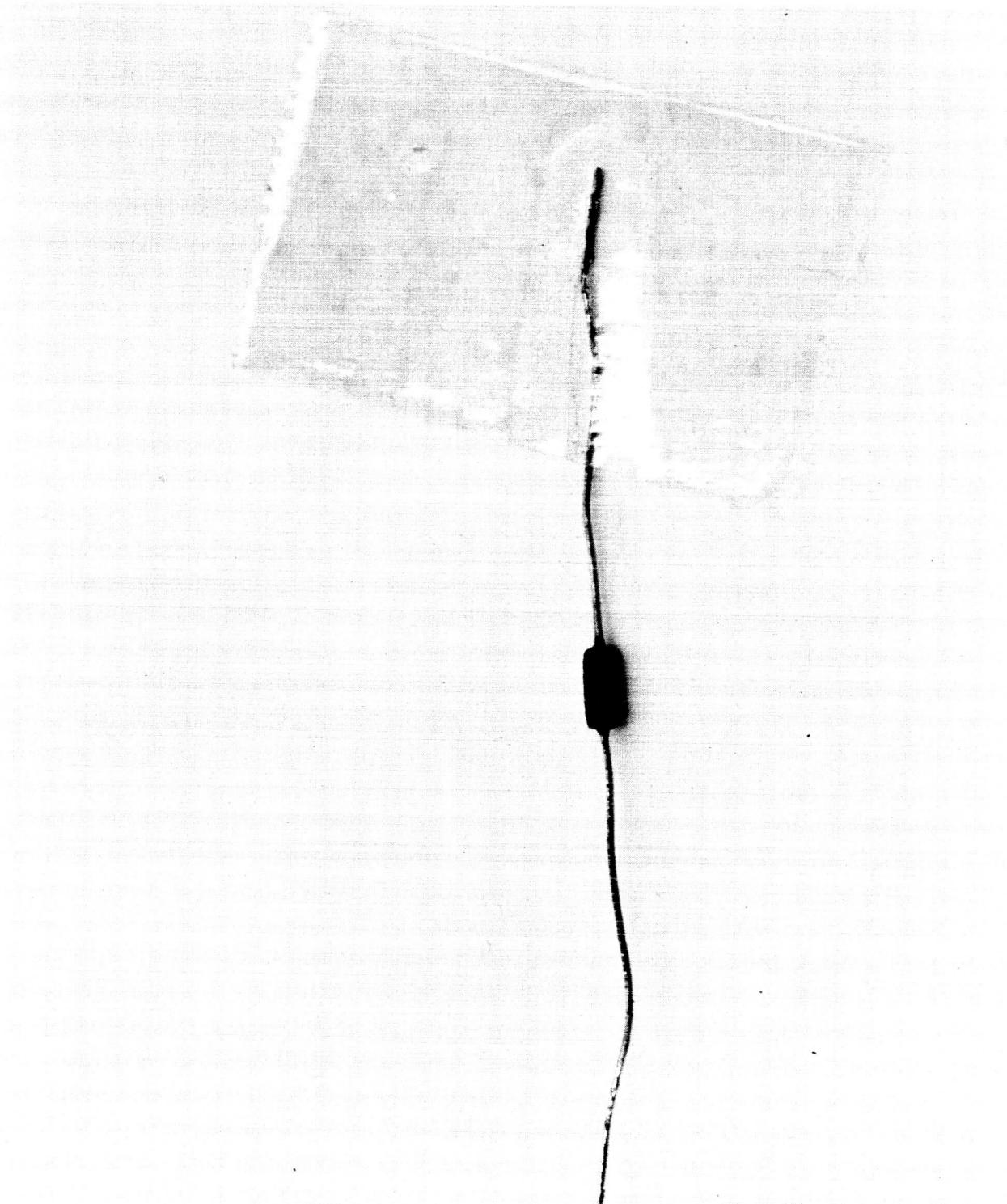


FIGURE 8 - MODEL TI-104A-200 ELEMENT



FIGURE 9 - MODEL TI-104A-200 INSERT ASSEMBLY

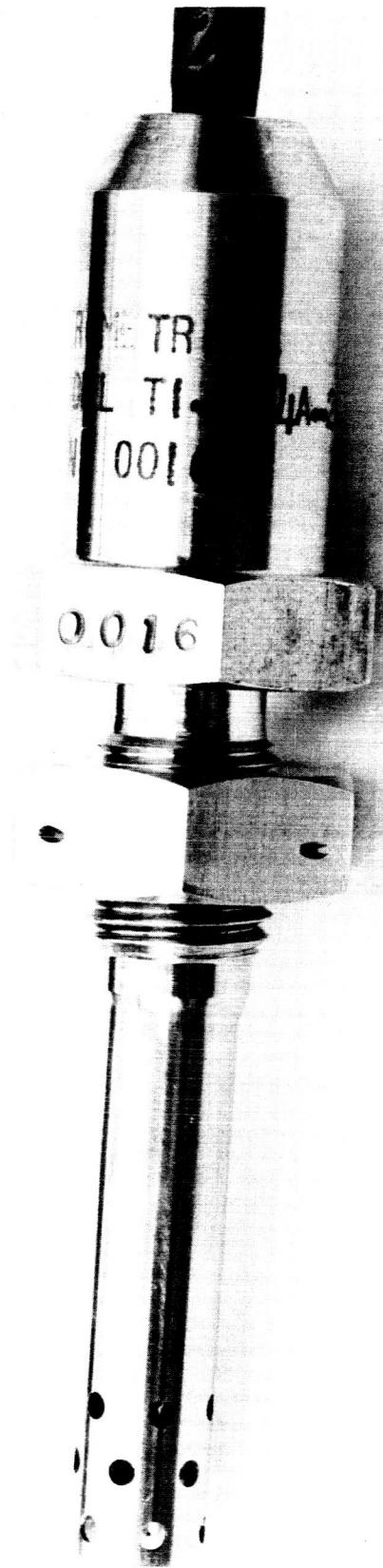


FIGURE 10 - MODEL TI-104A-200 TRANSDUCER



FIGURE 11 - MODEL TI-104A-200 TRANSDUCER

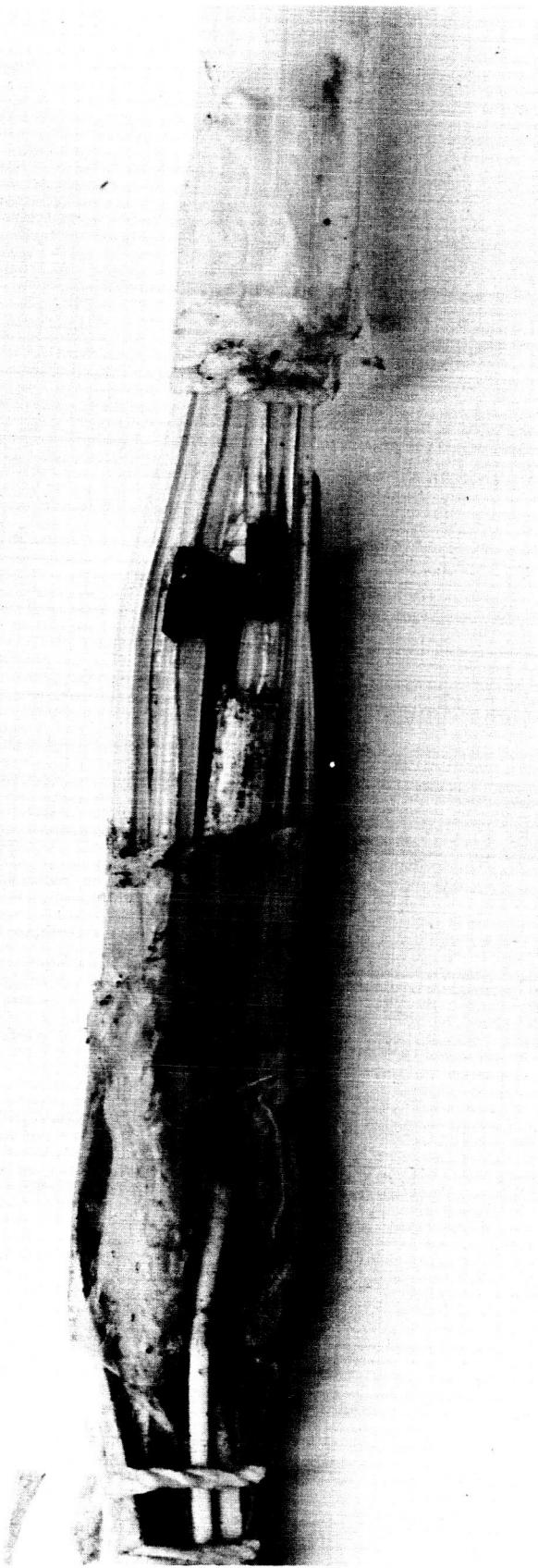


FIGURE 12 - FIVE ELEMENTS GROUPED TOGETHER WITH A
STANDARD FOR MULTIPONT CALIBRATION

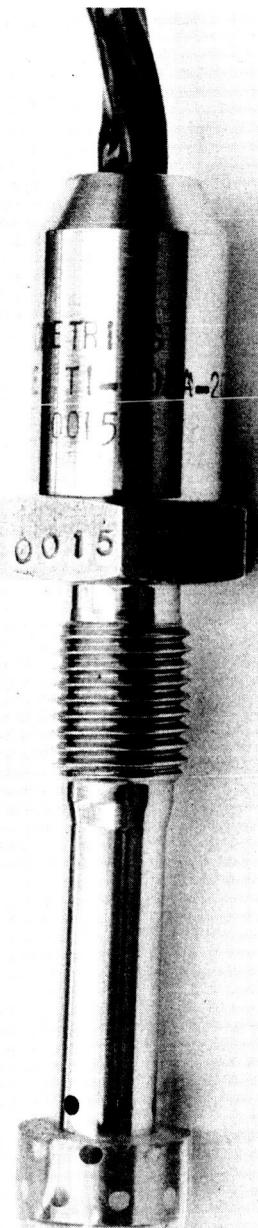


FIGURE 13 - MODEL TI-104A-200 PREPARED FOR RESPONSE TESTING IN LNe



FIGURE 14 - MODEL TI-104A-200 ELEMENT PREPARED FOR RESPONSE TESTING

(a) The element location at the tip varied slightly between the 5 pre-production prototype transducers.

(b) Two of the five transducers were fabricated with polished surfaces and the balance have vapor honed surfaces. The polished surface was selected for the final units.

(c) The elements were only calibrated in fixed point baths at 5 temperatures (ICE, CO₂, LN₂, LNe, and LHe) as compared with 10 temperatures for the production units.

2. Element Testing

Each of the resistors was tested to assure a stable ice point resistance by cycling from ambient to LN₂ for at least 10 cycles, and calibrated at five temperatures in fixed point baths. This data is reported in Enclosure 1. The greatest shift in resistance was 0.041 ohms or 0.041 percent which is acceptable per drawing 1126039.

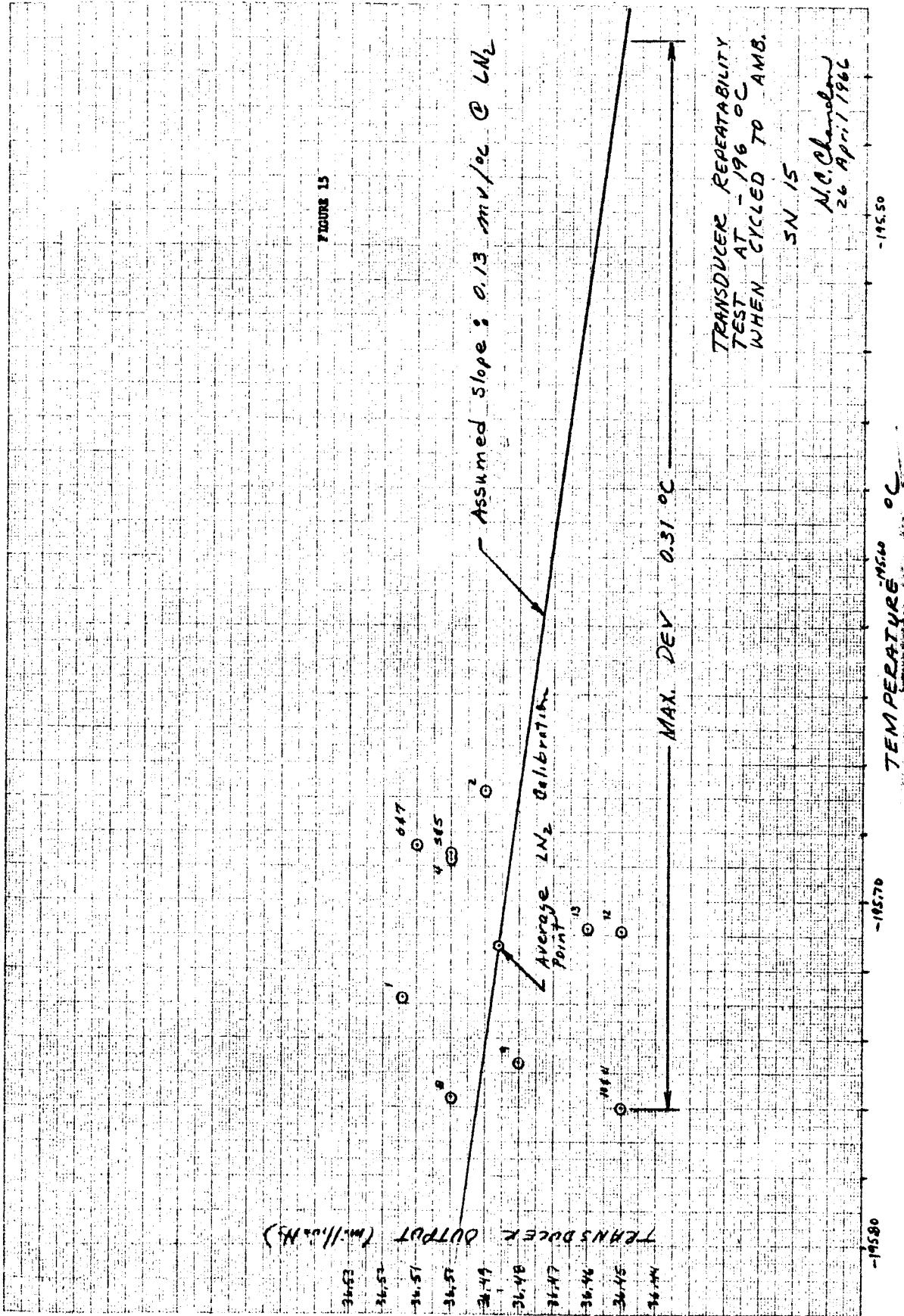
One of the elements, SN17, was response tested prior to fabrication into a completed transducer. Several experiments were conducted to acquire different characteristics of the element. Of primary interest is the response from LNe to GHe which corresponds to a step between LH₂ and GH₂. This data averaged 0.06 sec. (1TC) for 4 cycles.

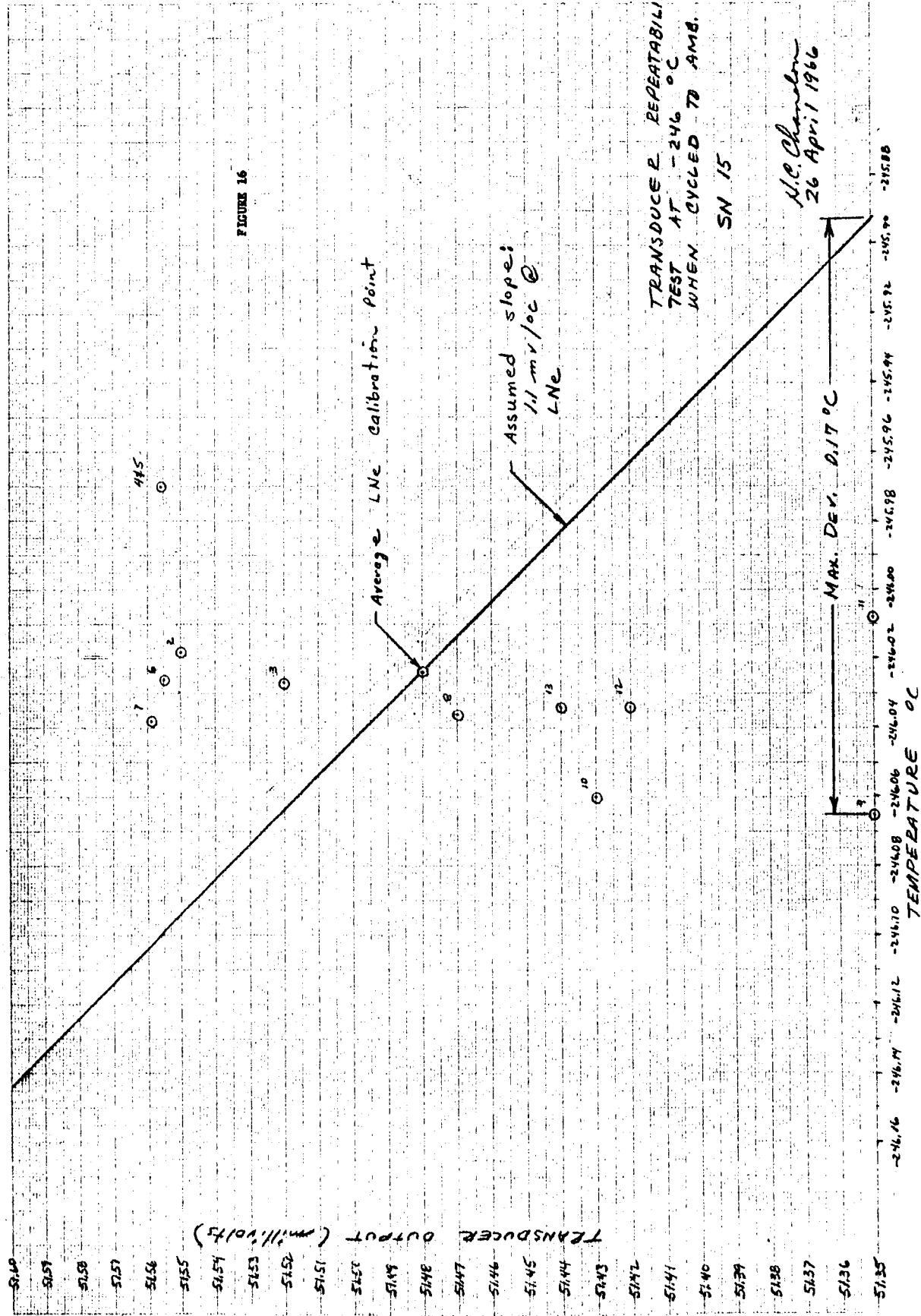
3. Transducer Testing

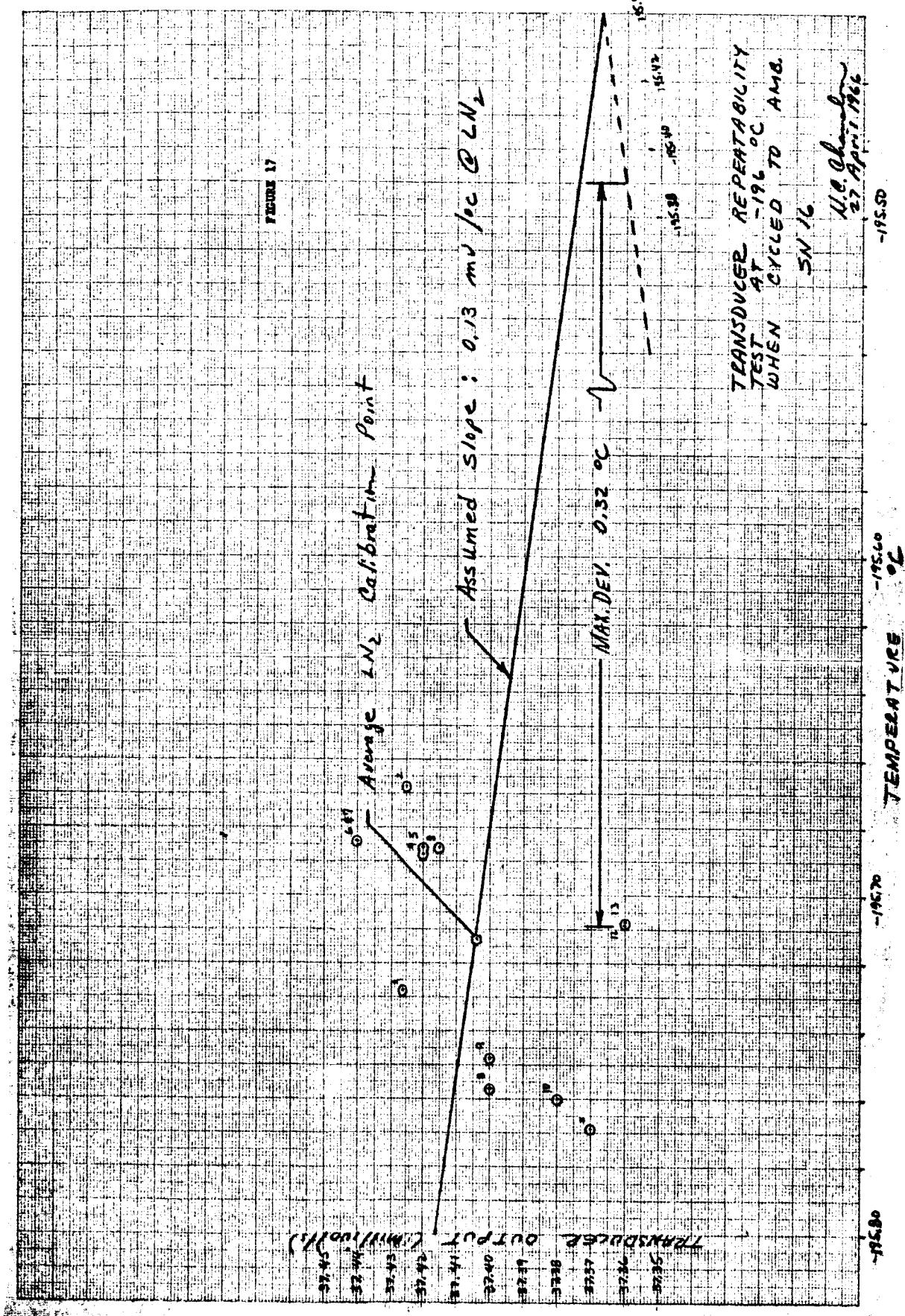
Each of the 5 pre-production prototype transducers was calibrated at four temperatures (ICE, ambient, LN₂ and LNe). The output measurements were taken using a constant current of 0.23 ma through the element. This data is recorded in Enclosure 2. This calibration data is insufficient to form a data reduction for the entire measurement range. Complete data reduction values will have to be calculated using the individual calibration data and the general curve shape from a typical curve for the production units.

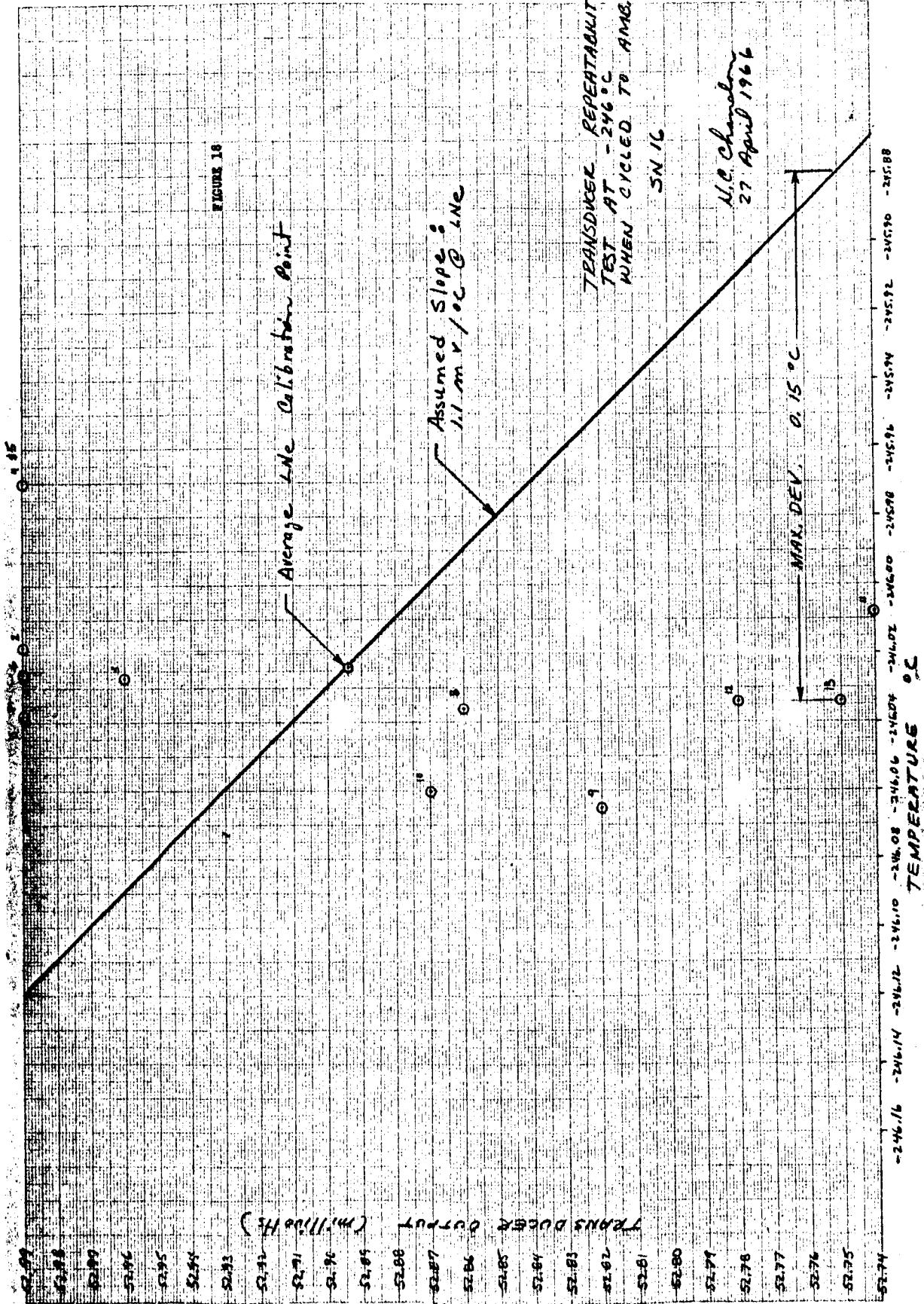
Response measurements were made on each of these transducers. The data is reported in Enclosure 2. This data must be correlated with the liquid hydrogen test data for establishing an alternate simple and cheap method of response testing.

Two of the transducers, SN 15 and 16, were cycled between ambient temperature and -246°C twelve times to evaluate the repeatability of the transducers. During each cycle, each transducer was calibrated at ambient, ICE, LN₂ and LNe temperatures. Graphical analysis, Figures 15 through 18, indicated the transducers to be repeatable 0.32°C at -246°C and 0.17°C at -196°C maximum. The assumed slope is the average value measured on the 13 production transducers. All the data are recorded in Enclosure 2.









D. PRODUCTION TRANSDUCERS

1. Introduction

A total of 13 transducers were fabricated and delivered to NASA. These transducers were fabricated in accordance with the following drawings, see Enclosure 3.

- a. 1126041 - Transducer, R/TC Temperature, Model TI-140A-200
- b. 1126040 - Insert, Thermocouple, Sub-Assembly, R/TC Temperature Transducer, Model TI-104A
- c. 1125449 - Nut, Drilled Jam
- d. 1126038 - Body, R/TC Temperature Transducer, Model TI-104A
- e. 1126037 - Stem and Insert, R/TC Temperature Transducer, Model TI-104A-200
- f. 1124976 - Tube, Protection
- g. 1126039 - Element, Resistor, R/TC Temperature Transducer, Model TI-104

2. Description

a. The transducer can be used as a totally immersed type, or for external use with the sensor protruding into the liquid through a boss. When used totally immersed, a jam nut is provided to allow mounting to a flat plate. For use through a boss, the jam nut is removed and an "O" ring installed for sealing.

b. The transducer housing, jam nut, stem and insert are made from type 321 stainless steel. (Figure 6)

c. A special teflon insulated four conductor cable is required for the transducer. The cable is composed of four conductors each of which is made up of five (5) strands of #26 AWG wire to form a #19 AWG conductor. There are two copper conductors, which provide excitation current to the resistor, one chromel thermocouple conductor and one constantan thermocouple conductor. Each conductor is reduced to one #26 AWG wire to allow direct mounting of the resistor to the wires in the stem of the transducer. (Figure 7)

d. The element is a sealed and calibrated 1/8 watt Allen Bradley carbon resistor mounted to provide a fast response in hydrogen. (Figure 8)

e. The lead wires are secured in the housing by a cryogenically compatible potting compound. (Figure 9)

f. To allow hydrogen flow around the element, the stem is perforated in a pattern which allows easy exit of generated gases and causing a pumping action on the liquid. This stem is required to provide mechanical protection for the element, and as a coupling means for attachment of the transfer tube used for response testing. (Figures 10 and 11)

3. Element Testing

Elements were prepared as detailed on drawing 1126039. Each element was scraped clean and then moisture sealed before any electrical testing was performed. All test data for the elements is attached as **Enclosures 4 and 5**.

Briefly, each element was tested first for repeatability before any calibrations were attempted. By this procedure, all elements which failed to meet the repeatability test, indicating a poor moisture seal or other impairment, were discarded as not acceptable as transducer elements. The repeatability was determined by measuring the ice point resistance for each of ten (10) cycles to liquid nitrogen.

The acceptable elements were then calibrated at several points within the normal operating range. Five elements were grouped together with a platinum resistance standard for this calibration. The temperatures were supplied by fixed point baths, the liquid helium controllable cryostat, and a hot air furnace as noted on the data sheets. The resistance of the element was measured using a four wire circuit with an excitation current of 0.25 milliamperes.

4. Acceptance Testing

Each production transducer (Figure 10) was tested in accordance with the Aerojet Test Procedure ATP-7905-007 (Enclosure 6). The data sheets generated during this testing are found as Enclosure 7.

The procedure calls for a final transducer calibration at five temperatures. The elements used in the transducer were previously calibrated, but since the element was mounted in the transducer after this calibration, and since the element is soldered to the lead wires during assembly, it is necessary to final calibrate to detect any shifts. The soldering of the lead wires to the resistor is a critical phase of the transducer fabrication since the joint thus formed is only 0.05 inches from the carbon composition resistor. The data generated by the five calibration points is sufficient to allow curve adjustment of the final transducer to meet the specified temperature accuracy required.

Response testing of each transducer was conducted using liquid neon (-246°C) or liquid nitrogen (-197°C) as the cryogenic medium. The response time was measured for changes in temperature from -246°C to -196°C and from -196°C to -246°C by either plunging the transducer from LN_2 to LNe, or immersing the sensor in LNe and blowing the LNe from around the element with gas conditioned to LN_2 temperature (Figure 13). Response data is shown in Enclosure 7.

5. Thermocouple Tables

With no excitation current to the transducer, each transducer output was measured during the acceptance testing. This data was used to develop a special EMF vs temperature table for the chromel constantan wire. Since the wire is from one spool, the average values are used to develop the most accurate set of tables. This temperature table is shown in Enclosure 8.

6. Calibration Data Sheets

A calibration data sheet for each transducer has been prepared. This data specifies the transducer output when using a constant current excitation of 0.23 ma for both no load and a 100k ohm load. Columns (2), (3), (10) and (16) provide the required data for using the developed transducer for temperature measurements. For greatest data reduction accuracy, the data should be programmed for reduction by a computer. For temperatures in the -253°C to -190°C range, data should be reduced using column (3) or logarithmic interpolation. For temperatures in the -190°C to $+60^{\circ}\text{C}$ range, data should be reduced using column (2) or linear interpolation.

Correction curves necessary to adjust for element resistance changes are enclosed. These values compensate for the element shift during assembly into the transducer presumably caused by soldering. See Enclosure 10.

E. TOOLING

A reference junction and ice bath were fabricated to aid in the checkout and operation of the transducers. Both of these parts were delivered with the production transducers.

The ice bath is a modified commercial 2 quart vacuum bottle. The cup was modified to seal the containing area and retain the reference thermocouple. When properly prepared, the bath will hold a stable temperature for 48 hours in a laboratory.

The reference junction is an immersion type designed to be used with the ice bath to provide a stable reference voltage for the transducers. Cable for the reference junction is from the same spool of wire as the transducers thus minimizing the splice junction errors.

These components are illustrated in Figures 19, 20 and 21. Fabrication drawings are attached as Enclosure 11.



FIGURE 19 - ICE BATH AND MODEL RJ-100 REFERENCE JUNCTION THERMOCOUPLE

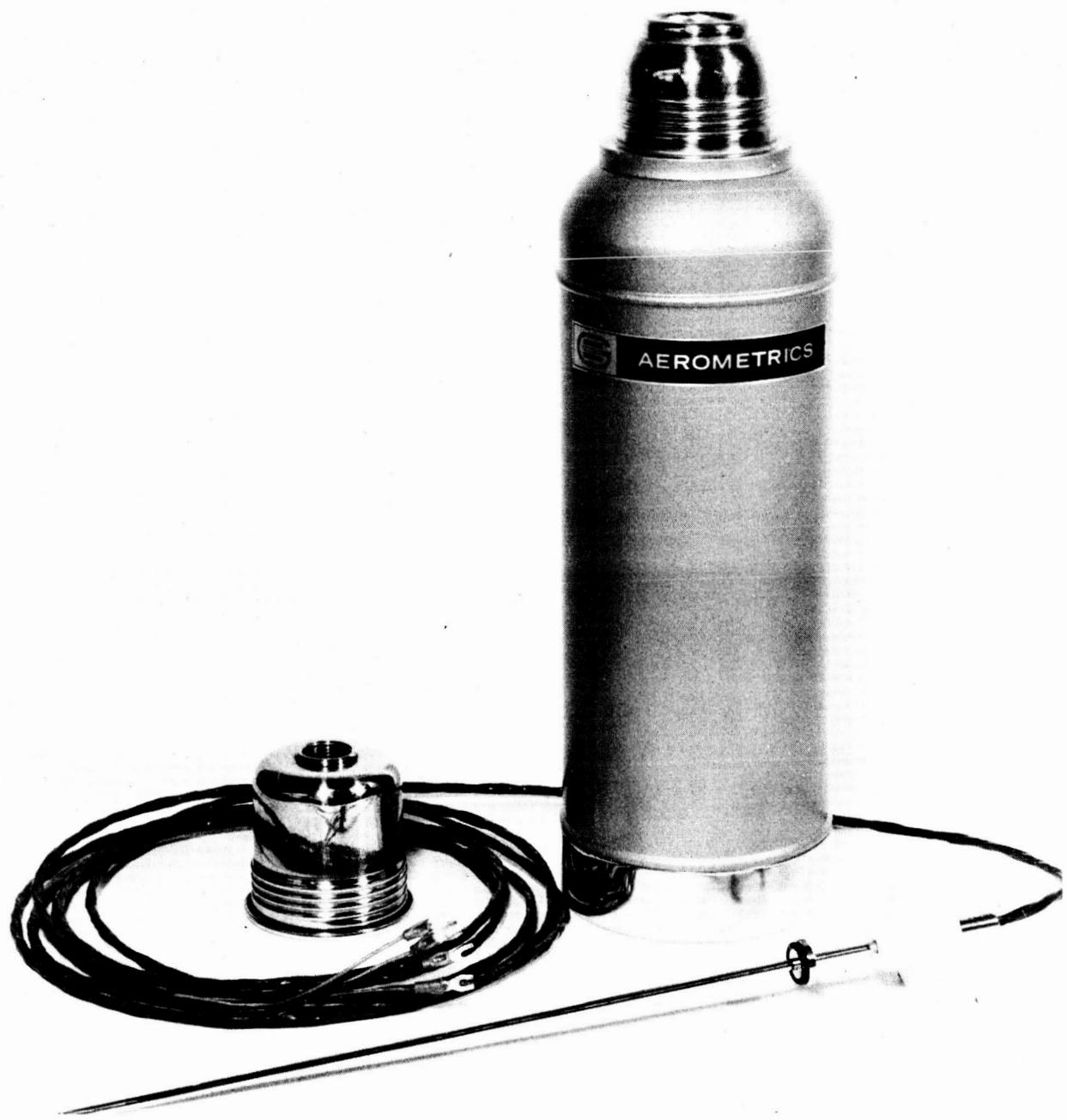


FIGURE 20 - ICE BATH AND MODEL RJ-100 REFERENCE JUNCTION THERMOCOUPLE

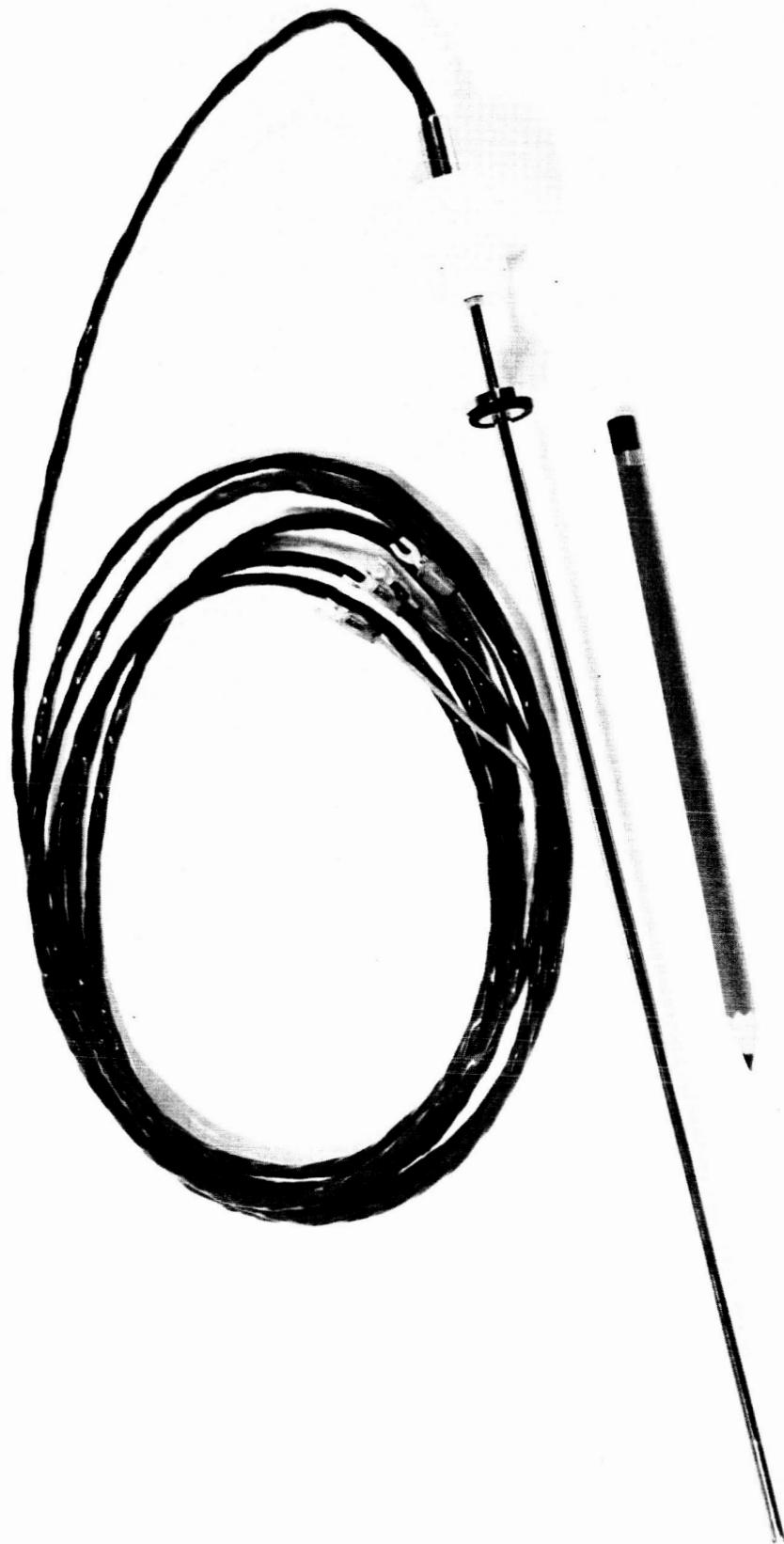


FIGURE 21 - MODEL RJ-100 REFERENCE JUNCTION THERMOCOUPLE

Enclosure 1
0700:1161

ELEMENT TEST DATA FOR
PRE-PRODUCTION PROTOTYPE TRANSDUCERS

CALIBRATION DATA SHEET

ICE TO LN₂ REPEATABILITY

DATE NOV 11 1965

ABC 1-028-008

MANUFACTURER

ALP

MODEL NO.
10012-32 1/8W

SERIAL NO.

PROOFING SHEET NO.

• 160

OV 11 1965

7A | 308

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED NOV 11 1965 (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES		
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)	
	TEST CYCLES	N	R	AVER				
1	98.181	98.201	98.191					
2	98.198	98.215	98.207					
3	98.213	98.235	98.224					
4	98.215	98.231	98.223					
5	98.216	98.237	98.227					
6	98.211	98.228	98.220					
7	98.216	98.238	98.227					
8	98.225	98.239	98.232					
9	98.223	98.239	98.231					
10	98.225	98.237	98.231					
						10 NT AVER 98.2212		
						0.091 DEVIATION		

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ICE TO LN₂ REPEATABILITY

DATE 11-15-1965

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ICE TO LN₂ REPEATABILITY

DATE NOV 16 1965

ABC 3-028-004

ALP

MODEL NO. 100±5% 1/8W

SERIAL NO 15

PROCEDURE NO.

TECHNICIAN

1

7A 30B

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ICE TO LN₂
REPEATABILITY

DATE NOV 18 1965

ABC 3-029-925

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES		
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)	
		NOV 18 1965	N	R	AVER			
		1	100.009	100.029	100.019			
		2	100.000	100.020	100.010			
		3	100.020	100.030	100.025			
		4	100.023	100.042	100.032			
		5	100.019	100.035	100.027			
		6	100.031	100.048	100.039			
		7	100.030	100.045	100.039			
		8	100.028	100.044	100.036			
		9	100.019	100.037	100.023			
		10	100.030	100.048	100.039			
						10 PT AVER. 100.029 ± 0.029 ± DEVIATION		

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ICE TO LN₂
REPEATABILITY

NOV 19 1965

ABC 3-028-005

MANUFACTURER

APL

MODEL N

$100.02 \pm 5\%$ 1/86

N-NO

17

卷之三

PROCEDURE NO.
0965-01-100

1

TECHNICIAN
R 7A 308

CALIBRATION DATA

(CONTINUED ON REVERSE SIDE)

ELEMENT CALIBRATION

CALIBRATION DATA SHEET

DATE JAN 10 1966

MANUFACTURER		MODEL NO.	SERIAL NO.	PROCEDURE NO.	TECHNICIAN	MANUFACTURER			
MANUFACTURER		MODEL NO.	SERIAL NO.	RECALL DATE	EQUIPMENT MANUFACTURER	MODEL NO.	SERIAL NO.	RECALL DATE	MANUFACTURER
PROC STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE NOMINAL (3)	MEASURED °K (4)	CORRECTED VALUE OF COLUMN (5)	✓ CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES LOWER LIMIT (7)	UPPER LIMIT (8)	MODEL NO.	
100/K	30 DEC 65	STO. TEMP 10	STO. TEMP 10	STO. TEMP 10	RT	Ratio	Inverse		
0.366099	ICE	273.15	—	32.000	97.824	1.0	0.366099		
0.513561	CO ₂	194.719	-78.431	-109.176	100.474	1.027083	0.513561		
1.292207	N ₂	77.387	-195.763	-320.379	122.350	1.250703	1.292207		
3.704526	INC	26.994	-246.156	-411.081	185.430	1.895528	3.704526		
—	ICE	273.15	—	32.000	97.826	1.0	—		

(CONTINUED ON REVERSE SIDE)

ELEMENT CALIBRATION

CALIBRATION DATA SHEET

DATE JAN 10 1966

CALIBRATION DATA

(CONTINUED ON REVERSE SIDE)

ELEMENT CALIBRATION

LINEAR DATA RECORD

AGCS 0711-36

DATE FEB - 3 1966

(CONTINUED ON REVERSE SIDE)

ELEMENT CALIBRATION

LINEAR DATA RECORD

AGCS 071136

113

(CONTINUED ON REVERSE SIDE)

LINEAR DATA RECORD

AGCS 0711-36

ELEMENT CALIBRATION

FEB - 3 1966

CALIBRATION DATA

(CONTINUED ON REVERSE SIDE)

ELEMENT

LINEAR DATA RECORD RESPONSE STUDY

AGCS 0711-36

19 Jan 1966

CALIBRATION DATA

	ITC (Sec.)	5TC (Sec.)			
Amb. to LN ₂	1.1	2.95			
	1.1	3.10			
	0.8	2.55			
	1.1	3.00			
av.	1.02	2.90			
Amb to LN ₂	0.9	3.10			
	0.8	2.75			
	1.0	3.40			
av.	0.90	3.08			
Amb to LNe	1.65	5.80			
	1.70	5.60			
	1.60	5.00			
	1.50	5.50			
av.	1.61	5.48			
LN ₂ to LNe	0.17	1.85			
	0.14	1.40			
	0.15	1.65			
	0.20	2.00			
av.	0.17	0.35			
LNe to GHe	0.08	0.16			
	0.05	0.11			
	0.06	0.12			
	0.06	0.12			
av.	0.06	0.13			

{CONTINUED ON REVERSE SIDE}

Enclosure 2
0700:1161

PRE-PRODUCTION PROTOTYPE

TRANSDUCER TEST DATA

CALIBRATION DATA
PREFPRODUCTION PROTOTYPE
TRANSDUCERS

25 APRIL 1966

	Temp. °K	Temp. °C	← no excitation no load	Output mv	→ Ic = 0, 2300 ma
			100K load	no load	100K load
SN 13	41.1111				
ICe	—	0	-0.046	-0.046	22.555
AMB	—	23.733	-1.455	-1.452	21.122
LN ₂	77.368	-195.782	8.604	8.587	36.741
LNe	27.180	-245.970	9.545	9.526	52.045
SN 14	41.1111				
ICe	—	0	-0.044	-0.044	22.340
AMB	—	23.733	-1.441	-1.380	20.914
LN ₂	77.368	-195.782	8.640	8.627	36.560
LNe	27.180	-245.970	9.589	9.569	51.640
SN 15	3.8133 11.66				
Av. of {	ICe	—	0	-0.037	22.321
13 ~ } AMB	—	23.124	-1.412	—	20.913
LN ₂	77.437	-195.713	8.608	—	36.486
LNe	27.126	-246.024	9.554	—	51.480
SN 16	3.8133 11.66				
Av. of {	ICe	—	0	-0.033	23.057
13 ~ } AMB	—	23.124	-1.415	—	21.653
LN ₂	77.437	-195.713	8.623	—	37.404
LNe	27.126	-246.024	9.577	—	52.894
SN 17	41.1111 11.66				
ICe	—	0	-0.034	-0.034	22.320
AMB	—	24.023	-1.377	-1.375	20.970
LN ₂	77.413	-195.737	8.633	8.621	36.570
LNe	26.996	-246.154	9.595	9.576	52.030
					51.920

(CONTINUED ON REVERSE SIDE)

LINEAR DATA RECORD

AGCS 0711-36

**RESPONSE TEST DATA
PREPRODUCTION PROTOTYPE
TRANSDUCERS**

25 APRIL 1966

MANUFACTURER		MODEL NO.	SERIAL NO.	PROCEDURE NO.		TECHNICIAN	DATE	
		Aerometrics TI-104A-200 As Noted				R	J	T
				CALIBRATION	EQUIPMENT			
MANUFACTURER	MODEL NO.	SERIAL NO.	RECALL DATE	MANUFACTURER	MODEL NO.	SERIAL NO.	RECALL DATE	MANUFACTURER
CALIBRATION DATA								
		SN 13	SN 14	SN 15	SN 16	SN 17		
		1TC	1TC	1TC	1TC	1TC		
		(sec)	(sec)	(sec)	(sec)	(sec)		
$L N_2$ to $L N_e$		0.22	0.19			0.23		
4T, L-66		0.27	0.20			0.21		
av.		0.29	0.22			0.18		
		—	—			0.19		
		0.26	0.20			0.20		
$L N_e$ to $G H_e$		0.21	0.11			0.11		
150 CFH $G H_e$		0.24	0.10			0.13		
flow 4T, L-66		0.24	0.12			0.09		
		—	—			0.09		
av.		0.23	0.11			0.11		
$A M B$ to $L N_2$				1.4	1.45			
19 Jan 66				1.4	1.5			
				1.55	—			
av.				1.45	1.48			
$A M B$ to $L N_e$				2.6	3.2			
19 Jan 66				2.9	2.95			
				2.8	—			
av.				2.76	3.08			
$L N_2$ to $L N_e$				0.20	0.25			
19 Jan 66				0.16	0.17			
				0.20	—			
av.				0.19	0.21			
$L N_e$ to $G H_e$				0.12	0.1			
19 Jan 66				0.10	0.14			
120 CFH $G H_e$				0.13	—			
flow				0.13	—			
				0.12	0.12			
av.								

(CONTINUED ON REVERSE SIDE)

TRANSDUCER
LINEAR DATA RECORD REPEATABILITY TEST
AGCS 0711-36

SHEET 1 OF 2

25 APRIL 1966

MANUFACTURER

DATE 25 APRIL 1966

CALIBRATION DATA						
	Fixed Point Calibration Media	Temp. K	Temp. C	Temp. F	RTT (m/s)	Tc (m/s)
27.Jan.1966	1 ICE				22,340	-0,016
	AMB	23,516	74,328	21,100	36,514	8,645
	LN ₂	77,422	-195,728		22,340	-0,016
28.Jan.1966	1 ICE				22,340	-0,016
	AMB	23,450	74,210	20,910	36,490	8,637
	LN ₂	77,486	-195,668		51,550	9,604
	LNe	27,132	-246,018		22,340	-0,016
29.Jan.1966	1 ICE				20,910	-1,402
	AMB	23,423	74,161	36,500	36,500	8,640
	LN ₂	77,464	-195,686		51,520	9,601
	LNe	27,123	-246,027		22,339	-0,016
30.Jan.1966	1 ICE				20,820	-1,470
	AMB	24,215	75,589	36,500	36,500	8,639
	LN ₂	77,462	-195,688		51,556	9,600
	LNe	27,180	-245,970		22,320	-0,015
31.Jan.1966	1 ICE				20,900	-1,430
	AMB	23,544	74,379	36,500	36,500	8,640
	LN ₂	77,464	-195,686		51,556	9,600
	LNe	27,180	-245,970		22,320	-0,025
32.Jan.1966	1 ICE				20,919	-1,398
	AMB	23,167		36,510	36,510	8,640
	LN ₂	77,466	-195,684		51,555	9,600
	LNe	27,124	-246,026		22,320	-0,020
33.Jan.1966	1 ICE				20,918	-1,400
	AMB	23,167		36,510	36,510	8,640
	LN ₂	77,466	-195,684		51,559	9,600
	LNe	27,112	-246,038			

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(CONT.)

LINEAR DATA RECORD REPEATABILITY TEST

LINEAR
AGCS 0711-36

TRANSDUCER

REPEATABILITY

SHEET 2 OF 2

25 APRIL 1966

CALIBRATION DATA						
	Fixed Point Calibration Media	Temp. K	Temp. C	Temp. F	RTT (mV)	TC (mV)
8	ICE				22,320	-0,060
	AMB		23,168		20,917	-1,400
	LN ₂	77,393	-195,757		36,500	8,580
9	LNE	27,114	-246,036		51,470	9,550
	ICE				22,310	-0,055
	AMB		23,452		20,850	-1,468
10	LN ₂	77,403	-195,747		36,480	8,572
	LNE	27,085	-246,065		51,350	9,500
	ICE				22,310	-0,055
11	AMB		23,027		20,964	-1,375
	LN ₂	77,390	-195,760		36,450	8,562
	LNE	27,090	-246,060		51,430	9,500
11-11-11-11		ICE			22,310	-0,055
12	AMB		22,285		20,860	-1,455
	LN ₂	77,381	-195,769		36,450	8,550
	LNE	27,142	-246,008		51,350	9,490
21-11-11-11		ICE			22,300	-0,055
13	AMB		22,639		20,894	-1,426
	LN ₂	77,441	-195,709		36,450	8,578
	LNE	27,116	-246,034		51,420	9,502
21-11-11-11		ICE			22,310	-0,055
Average	AMB		22,565		20,910	-1,406
	LN ₂	77,442	-195,708		36,460	8,580
	LNE	27,116	-246,034		51,440	9,504
Average		ICE			22,315	-0,056
↓	AMB		23,124		20,913	-1,412
	LN ₂	77,437	-195,713		36,486	8,608
	LNE	27,126	-246,024		51,480	9,554

TRANSDUCER
LINEAR DATA RECORD REPEATABILITY TEST
AGCS 0711-36

SHEET 1 OF 2

DATE 26 APRIL 1966

MANUFACTURER

CALIBRATION DATA						
	Fixed Point Calibration Media	Temp. K	Temp. C	Temp. F	RTT (mV)	TC (mV)
27 Jun. 1966	ICE				23,060	-0,014
	AMB		23,516	74,328	21,760	-1,400
	LN ₂	77,422	-195,728		37,426	8,645
28 Jun. 1966	ICE				23,060	-0,014
	AMB		23,450	74,210	21,630	-1,410
	LN ₂	77,486	-195,668		37,425	8,658
29 Jun. 1966	LNe	27,132	-246,018		52,990	9,630
	ICE				23,065	-0,014
	AMB		23,423	74,161	21,640	-1,390
30 Jun. 1966	LN ₂	77,464	-195,686		37,415	8,656
	LNe	27,123	-246,027		52,960	9,628
	ICE				23,070	-0,005
31 Jun. 1966	AMB		24,215	75,589	21,570	-1,490
	LN ₂	77,462	-195,688		37,420	8,660
	LNe	27,180	-245,970		52,990	9,635
1 Jul. 1966	ICE				23,070	-0,006
	AMB		23,544	74,379	21,620	-1,480
	LN ₂	77,464	-195,686		37,420	8,660
2 Jul. 1966	LNe	27,180	-245,026		52,990	9,634
	ICE				23,080	-0,010
	AMB		23,167		21,660	-1,393
3 Jul. 1966	LN ₂	77,466	-195,686		37,440	8,650
	LNe	27,180	-245,970		52,990	9,630
	ICE				23,080	-0,015
4 Jul. 1966	AMB		23,167		21,660	-1,395
	LN ₂	77,466	-195,684		37,440	8,650
	LNe	27,112	-246,038		52,990	9,630

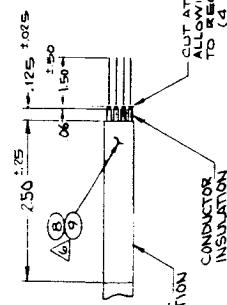
(CONTINUED ON REVERSE SIDE)

Enclosure 3
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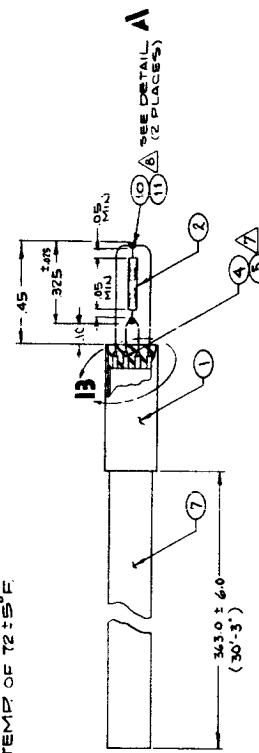
**FABRICATION DRAWINGS FOR
PRODUCTION TRANSDUCERS**

4 | 3 | 2 | 1

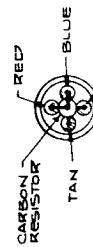
NOTES:		D		C		B		A	
1. REMOVE ALL BURRS & SHARP EDGES.									
2. INTERPRET DWG. PER STD'S PRESCRIBED IN MIL-D-7032Z.									
3. CLEAN TO LEVEL "H" PER AGC-46350.									
4. PRESERVE & PACKAGE PER AGC-46367, CLASS I.									
5. MARK PER AND SCREEN WITH PN 1126040 & APPLICABLE DASH NO.									
6. CABLE + CONDUCTOR TO BE EPOXY BOND TREATED PER MIL-C. INSTRUCTIONS USING HEAT DRYING.									
7. ENDY SMALL BE 50% SO% MIXTURE BY VOLUME CURED AT 125° ± 15°F FOR 6 HRS. MINIMUM.									
8. WIRES ARE TO BE PREFORMED & SOLDERED TOGETHER WITH MINIMUM AMOUNT OF SOLDER. NEXT INSTALL RESISTOR & SOLDER IN PLACE USING COPPER HEAT SINKS BETWEEN RESISTOR BODY & SOLDER JOINT TO ASSURE MINIMUM HEAT TRANSFER TO RESISTOR BODY.									
9. DURING CABLE PREPARATION & ASSEMBLY, HANDLE WITH CLEAN HANDS & AVOID EXCESSIVE BENDING OF WIRES.									
10. ELECTRICAL CONTINUITY TESTS SHALL BE PERFORMED ON EACH UNIT AT AMBIENT TEMP OF 72 ± 5°F.									
BLUE TO BLACK - BETWEEN 95 - 105 OHMS									
RED TO BLUE - BETWEEN 0 - 11 OHMS									
TAN TO BLACK - BETWEEN 11 - 14 OHMS									
RED TO INSERT - GREATER THAN 100 MEGOMHS AT 50V DC.									



DETAIL D



— 9 ASSEMBLY —



ELEMENT CONSTRUCTION
END VIEW
DETAIL A



— SCHEMATIC —

REF ID	DESCRIPTION	QUANTITY		NOTES
		UNIT	AMOUNT	
A	TRANSISTOR, NPN, THEROCOUPLE SUB ASSEMBLY	PCB	1	
B	R/TC, THEROCOUPLE SUB ASSEMBLY	PCB	1	
C	R/TC, THEROCOUPLE SUB ASSEMBLY	PCB	1	
D	TRANSISTOR, MODEL TS-104A SUB ASSEMBLY	PCB	1	
	LIST OF MATERIALS			
	1. CARBON RESISTOR 2. CHROMEL 3. COPPER 4. TAN			
	5. THEROCOUPLE 6. TRANSISTOR 7. POLYMER COAT			
	8. FLUX	FLUX	1	
	9. V-SMOOTH SOLDER	SOLDER	1	
	10. AD-BOND	AD-BOND	1	
	11. HARMON	HARDWARE	1	
	12. SANTA ANA, CALIF	SANTA ANA, CALIF	1	
	13. 1126040	1126040	1	

790
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2
3
4

1

2

3

4

790

1

2

3

4

- D
 1 REMOVE ALL BURRS & SHARP EDGES.
 2 INTERPRET DWG. PER STD'S PRESCRIBED IN MIL-D-70327.
 3 CLEAN TO LEVEL 'W' PER AGC 4C350.

4 PRESERVE & PACKAGE PER AGC 4C387, CLASS 1.

5 EPOXY SHALL BE 50% - 50% MIXTURE BY VOLUME
CURED AT 125° ± 5°F FOR 8 HRS MINIMUM.

6 AT ASSEMBLY REDUCE 292 DIAM ON ITEM 1 (PN 11260357-1) TO HAVE
A PRESS FIT (15 LBS MAX) WHEN MATED WITH ITEM 2 (PN 11260361)
FOR EASE OF WELDMENT.

7 TIG WELD PER AGC 4C351

8 MARK PER ASD 5215C

9 MARK PER ASD 5215D

10 ACCEPTANCE TESTS SHALL BE PERFORMED ON EACH UNIT MANUFACTURED PER
PROCEDURE NO. (TO BE PREPARED).

CAUTION - DO NOT EXPOSE THE RESISTOR TO ICE AND/OR
WATER. THE ICE POINT RESISTANCE SHALL BE
MEASURED BY IMMERSING THE RESISTOR
IN ETHANOL LIQUID AT 32.0 ± .05°F

SEE DETAIL A

B

SEE DETAIL B

C

SEE DETAIL C

D

SEE DETAIL D



FOLD BACK ALL STRANDS
OF WIRE & CRIMP.
SEAL BOTH ENDS WITH EPOXY \triangle
DETAIL A
NO SCALE

△
EPIXY SMALL BE 50% - 50% MIXTURE BY VOLUME
CURED AT 125° ± 5°F FOR 8 HRS MINIMUM.

△
AT ASSEMBLY REDUCE 292 DIAM ON ITEM 1 (PN 11260357-1) TO HAVE
A PRESS FIT (15 LBS MAX) WHEN MATED WITH ITEM 2 (PN 11260361)
FOR EASE OF WELDMENT.

△
TIG WELD PER AGC 4C351

△
MARK PER ASD 5215C

△
MARK PER ASD 5215D

11 INTERPRET DWG. PER STD'S PRESCRIBED IN MIL-D-70327.

12 PRESERVE & PACKAGE PER AGC 4C387, CLASS 1.

13 EPOXY SHALL BE 50% - 50% MIXTURE BY VOLUME
CURED AT 125° ± 5°F FOR 8 HRS MINIMUM.

14 AT ASSEMBLY REDUCE 292 DIAM ON ITEM 1 (PN 11260357-1) TO HAVE
A PRESS FIT (15 LBS MAX) WHEN MATED WITH ITEM 2 (PN 11260361)
FOR EASE OF WELDMENT.

15 TIG WELD PER AGC 4C351

16 MARK PER ASD 5215C

17 MARK PER ASD 5215D

18 SEE DETAIL A

B

SEE DETAIL B

C

SEE DETAIL C

D

SEE DETAIL D

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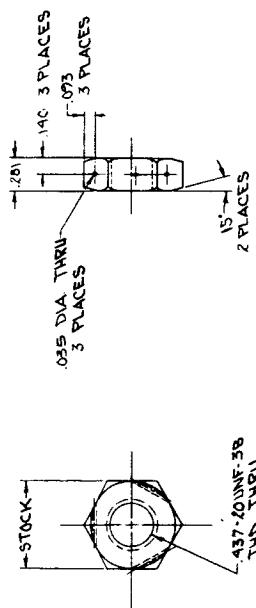
324

326

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329

D NOTES:
1 REMOVE ALL BURRS & SHARP EDGES.
2 INTERPRET DIMG PER STDG. PRESCRIBED IN MIL-D-70327.
3 CLEAN TO LEVEL "H" PER AGC-46350.
4 PRESERVE & PACKAGE PER AGC-46307, CLASS I.
5 ALL MACHINED SURFACES TO BE $\frac{3}{16}$ " OR BETTER.
6 MARK PER AS9521N WITH PN 1125449.



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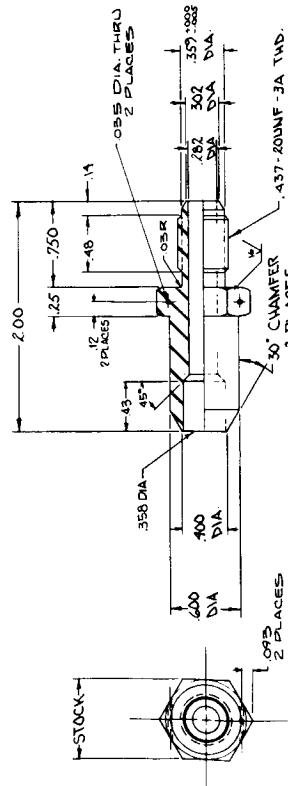
4

C

B

A

- NOTES:**
- D 1. REMOVE ALL BURRS & SHARP EDGES.
 2. INTERPRET DWG. PER STD'S. PRESCRIBED IN MIL-D-70327.
 3. CLEAN TO LEVEL "H" PER AGC-46350.
 4. PRESERVE & PACKAGE PER AGC-46387, CLASS I.
 5. MARK PER AND 5215N WITH PN 1126038.
 6. ALL MACHINED SURFACES SHALL BE $\frac{1}{16}$ OR BETTER.



REVISED TO REFLECT AS BUILT CONDITION		5-14-74 COA D&M

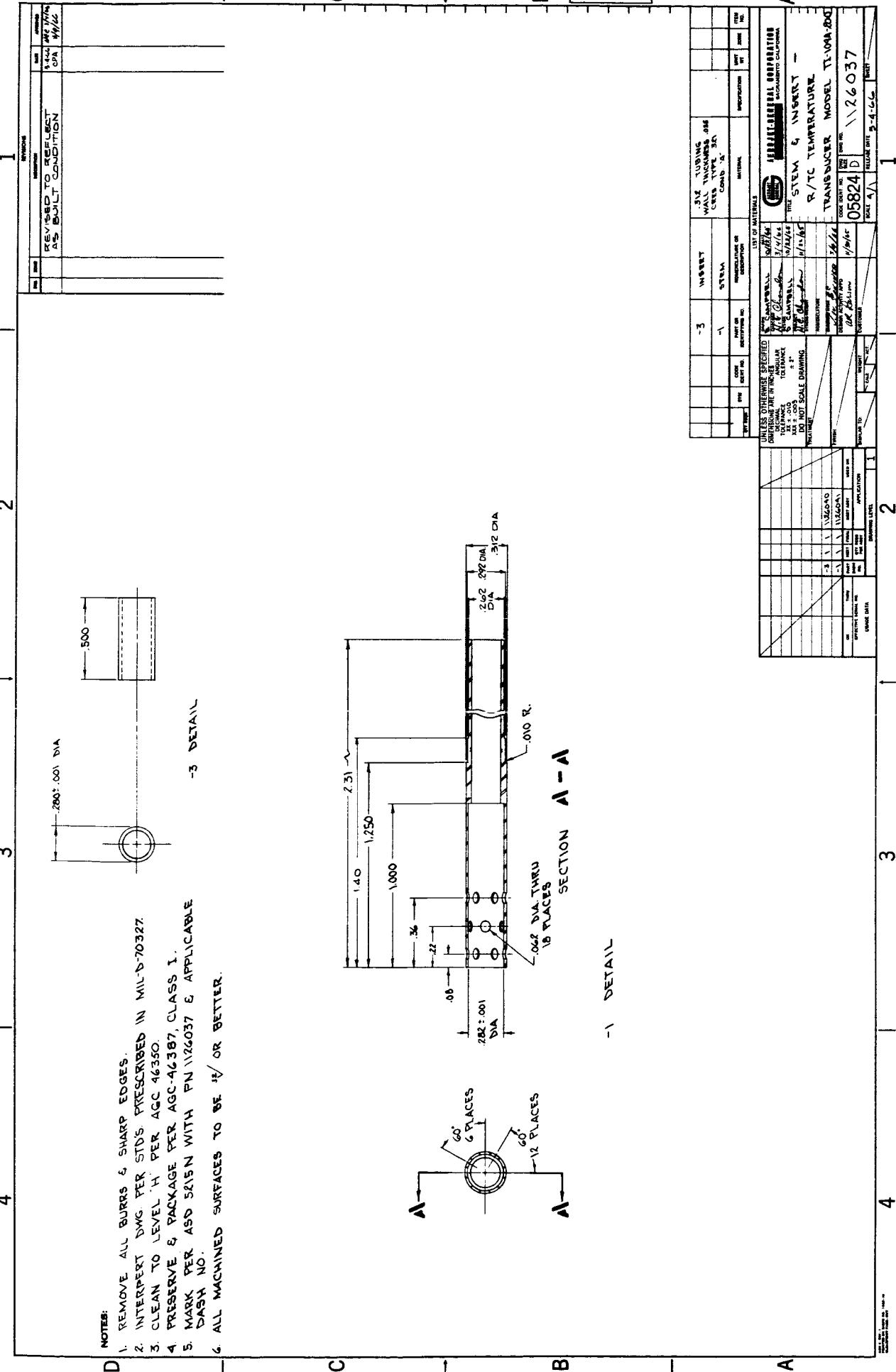
ITEM NO.	DESCRIPTION	75° USA GAGE CROWN TYPE 32A. MATERIAL		CONT. A SPECIFICATION	UNIT OF MEASURE
		ITEM NO.	ITEM NO.		
LIST OF MATERIALS					
1	1	-	-	-	-

TECHNICAL DRAWING REVISIONS		TECHNICAL DRAWING REVISIONS		TECHNICAL DRAWING REVISIONS	
1	1	1	1	1	1
2	2	2	2	2	2
3	3	3	3	3	3
4	4	4	4	4	4

1126038 D 1126038 D 1126038 D

1126038 D 1126038 D 1126038 D

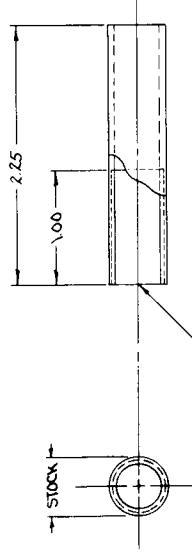
1126038 D 1126038 D 1126038 D



INSTRUCTIONS	
REVERSE TO REVERSE	3.4-10-74 CPA 10874
AS BUILT CONDITION	

1 2 3 4

- D NOTES:
- 1 REMOVE ALL BURRS & SHARP EDGES.
 - 2 INTERPRET DWG. PER STD'S PRESCRIBED IN MIL-D-70327.
 - 3 CLEAN TO LEVEL "H" PER AGC-A4350.
 - 4 MARK PER ASO 525N WITH PN 1124976.
 - 5 MACHINED SURFACES TO BE #4 OR BETTER



ITEM NO.	NAME	SIZE, WEIGHT, OR QUANTITY		SPECIFICATION	UNIT OF MEASURE	ZONE NO.
		ITEM NO.	NAME			
ITEM NO. 1 5824 D TUBE, PROTECTION						
1	5824 D	1	1	1	1	1
ITEM NO.	NAME	ITEM NO.	NAME	ITEM NO.	NAME	ITEM NO.
1	5824 D	1	1	1	1	1
ITEM NO.	NAME	ITEM NO.	NAME	ITEM NO.	NAME	ITEM NO.

2 3 4

1 2 3 4

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2

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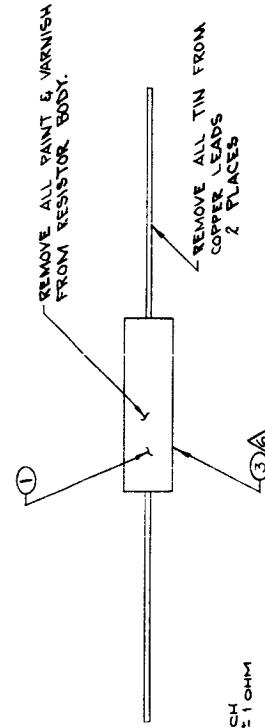
- D**
- NOTES:
- 1 REMOVE ALL BURRS & SHARP EDGES.
 - 2 INTERPRET DUG PER STD'S PRESCRIBED IN MIL-D-70327.
 - 3 CLEAN TO LEVEL "W" PER AGC-46350.
 - 4 PRESERVE & PACKAGE PER AGC-16387, CLASS Y.
 - 5 MARK PER AND 5215N WITH PN 1126039.

- ⚠️ APPLY RESIN WITH MIN THICKNESS, CURE UNDER PRESSURE OF 50 PSIG FOR TWO (2) HOURS AT AMBIENT TEMPERATURE, ($72^{\circ}\text{F} \pm 5^{\circ}\text{F}$) DRY AT 100°F FOR A MIN. OF 24 HOURS.

⚠️ ACCEPTANCE TEST SHALL BE PERFORMED ON EACH UNIT MANUFACTURED.

C

CAUTION - DO NOT EXPOSE THE RESISTOR TO ICE AND/OR WATER. THE ICE POINT RESISTANCE SHALL BE MEASURED BY IMMERSING THE RESISTOR IN ETHANOL LIQUID AT $212.00 \pm 0.05^{\circ}\text{F}$.



⚠️ ACCEPTANCE TEST

STEP 1 - PRE SELECTION
ONLY CURED AND TREATED RESISTORS WHICH HAVE AN ICE POINT RESISTANCE OF $97.5 \pm 1\text{ OHM}$ SHALL BE ACCEPTABLE.

STEP 2 - REPEATABILITY TEST

CYCLE EACH RESISTOR BETWEEN LIQUID NITROGEN & AMBIENT TEMP ($72 \pm 5^{\circ}\text{F}$) TEN TIMES. RECORD THE ICE POINT RESISTANCE BEFORE EACH CYCLE. ONLY RESISTORS WHICH REPEAT THE ICE POINT RESISTANCE WITHIN $\pm 0.05\text{ OHMS}$ OF THE INITIAL MEASUREMENT ARE ACCEPTABLE.

STEP 3 - PRE-CALIBRATION TESTS

MEASURE & RECORD THE RESISTANCE AT TEN TEMPERATURES WITHIN THE TEMPERATURE SPAN OF $+140$ TO -42°F .

B 6E092111 400

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	REVISION	AS BUILT CONDITION	
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REF ID	REVISED TO REFLECT		DATE
	REVISION	AS BUILT CONDITION	
1			
2			
3			

REF ID	REVISED TO REFLECT		DATE
	REVISION	AS BUILT CONDITION	
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2			
3			

REF ID	REVISED TO REFLECT		DATE
	REVISION	AS BUILT CONDITION	
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3			

REF ID	REVISED TO REFLECT		DATE
	REVISION	AS BUILT CONDITION	
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	REVISION	AS BUILT CONDITION	
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	REVISION	AS BUILT CONDITION	
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	REVISION	AS BUILT CONDITION	
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3			

REF ID	REVISED TO REFLECT		DATE
	REVISION	AS BUILT CONDITION	
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REF ID	REVISED TO REFLECT		DATE
	REVISION	AS BUILT CONDITION	
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2			
3			

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Enclosure 4
0700:1161

ELEMENT ICE TO LN₂ REPEATABILITY

TEST DATA FOR 13 PRODUCTION TRANSDUCERS

CALIBRATION DATA SHEET

ICE TO LN₂

DATE 061 28 1965

ABC 3-029-008

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CONNECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES		
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)	
		OCT 26 1965	N	R	AVER.			
		TEST CYCLES	1	96.959	96.979	96.969		
			2	96.968	96.985	96.977		
			3	96.972	96.992	96.982		
			4	96.969	96.986	96.978		
			5	96.961	96.979	96.970		
			6	96.963	96.984	96.974		
			7	96.960	96.978	96.969		
			8	96.972	96.992	96.982		
			9	96.964	96.984	96.974		
			10	96.972	96.992	96.982	10 PT. AVER 96.974	0.0142 DEVIATION
Acceptable		per drawing 1126039 (steps 1 and 2)			H.P. Chardron 9 March 66			

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET ICE TO LN₂

MANUFACTURER AEROMETRICS		MODEL NO 1126039	SERIAL NO 5	PROCEDURE NO	DATE NOV - 1 1965																																																																														
CALIBRATION EQUIPMENT TESTED																																																																																			
STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE NOMINAL (3)	MEASURED (4)	CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6) CALIBRATION TOLERANCES LOWER LIMIT (7) UPPER LIMIT (8)																																																																														
<p style="text-align: center;">CALIBRATION DATA</p> <table border="1"> <thead> <tr> <th colspan="2"></th> <th colspan="2"></th> <th colspan="2"></th> </tr> <tr> <th>PROC.</th> <th>STEP NO.</th> <th>N</th> <th>R</th> <th>AVER.</th> <th></th> </tr> </thead> <tbody> <tr><td></td><td>TEST CYCLES 1</td><td>96.558₂</td><td>96.576₂</td><td>96.567₂</td><td></td></tr> <tr><td></td><td>2</td><td>96.564</td><td>96.585</td><td>96.575</td><td></td></tr> <tr><td></td><td>3</td><td>96.571</td><td>96.589</td><td>96.580</td><td></td></tr> <tr><td></td><td>4</td><td>96.564</td><td>96.584</td><td>96.574</td><td></td></tr> <tr><td></td><td>5</td><td>96.579</td><td>96.595</td><td>96.587</td><td></td></tr> <tr><td></td><td>6</td><td>96.578</td><td>96.594</td><td>96.586</td><td></td></tr> <tr><td></td><td>7</td><td>96.577</td><td>96.592</td><td>96.585</td><td></td></tr> <tr><td></td><td>8</td><td>96.579</td><td>96.594</td><td>96.587</td><td></td></tr> <tr><td></td><td>9</td><td>96.578</td><td>96.593</td><td>96.586</td><td></td></tr> <tr><td></td><td>10</td><td>96.577₂</td><td>96.591₂</td><td>96.584₂</td><td>10 AT. AVER 96.581₂ 0.020₂ DEVIATION</td></tr> <tr><td colspan="6">Acceptable per dwg 1126039 (steps 1011 & 2) H. C. Chandola</td></tr> </tbody> </table>												PROC.	STEP NO.	N	R	AVER.			TEST CYCLES 1	96.558 ₂	96.576 ₂	96.567 ₂			2	96.564	96.585	96.575			3	96.571	96.589	96.580			4	96.564	96.584	96.574			5	96.579	96.595	96.587			6	96.578	96.594	96.586			7	96.577	96.592	96.585			8	96.579	96.594	96.587			9	96.578	96.593	96.586			10	96.577 ₂	96.591 ₂	96.584 ₂	10 AT. AVER 96.581 ₂ 0.020 ₂ DEVIATION	Acceptable per dwg 1126039 (steps 1011 & 2) H. C. Chandola					
PROC.	STEP NO.	N	R	AVER.																																																																															
	TEST CYCLES 1	96.558 ₂	96.576 ₂	96.567 ₂																																																																															
	2	96.564	96.585	96.575																																																																															
	3	96.571	96.589	96.580																																																																															
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	6	96.578	96.594	96.586																																																																															
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	9	96.578	96.593	96.586																																																																															
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Acceptable per dwg 1126039 (steps 1011 & 2) H. C. Chandola																																																																																			

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ANSWER: $\lambda = 0.25 = 0.05$

ICE TO Li_2

DATE NOV - 2 1965

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED H:AV - 1 1905 (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES	
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)
		Test Cycles	N	R	AVER		
		1	97.067	97.085	97.076		
		2	97.080	97.099	97.099		
		3	97.074	97.091	97.083		
		4	97.072	97.100	97.091		
		5	97.092	97.108	97.100		
		6	97.086	97.103	97.095		
		7	97.105	97.120	97.113		
		8	97.100	97.120	97.110		
		9	97.090	97.105	97.098		
		10	97.094	97.112	97.103	10 PT AVER	97.096
						0.03%LR DEVIATION	
		Acceptable per chart 110-139 (Steps 1 and 2.)		H.C. Chandon		9 March 66	

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ATE NOV - 5 1965

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

AAC 3-028-008

ACT 3-026-008

MANUFACTURER

MODEL NO.

SERIAL NO

PROCEDURE NO.

V - 8 1965

TECHNICIAN

8

CALIBRATION DATA

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ABC-3-221-205

CALIBRATION DATA

PROC. STEP NO.	NOV - 9 1965 FUNCTION TESTED	READING OR VALUE		CORRECTED VALUE OF COLUMN	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE	CALIBRATION TOLERANCES	
		NOMINAL (2)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)
	TEST CYCLES	N	R	AVER			
1	97.475	97.493	97.484				
2	97.503	97.521	97.512				
3	97.512	97.528	97.520				
4	97.512	97.531	97.522				
5	97.519	97.537	97.528				
6	97.519	97.539	97.529				
7	97.514	97.533	97.524				
8	97.513	97.535	97.524				
9	97.512	97.532	97.522				
10	97.517	97.537	97.527				
11	97.516	97.534	97.525				
12	97.519	97.537	97.528				
13	97.516	97.534	97.525				
14	97.515	97.532	97.524				
15	97.518	97.530	97.522				
16	97.517	97.534	97.525				
17	97.516	97.534	97.525				
18	97.518	97.530	97.522				
19	97.517	97.537	97.527				
20	97.516	97.534	97.525				
				20 AT AVER	97.522 ±		
	Acceptable per chart	1126030	(steps 1 and 2)		ΔR = 0.045 ±		
					H.C. Chamber - 7.11.166		

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ABC 2-088-008

DATE NOV 29 1965

MANUFACTURER	MODEL NO.	SERIAL NO.	PROCEDURE NO.	TECHNICIAN
HEROMETRICS	1126039	19		R 7A308
CALIBRATION EQUIPMENT				
(1) INSTRUMENT (2) MODEL NO. (3) SERIAL NO. (4) RECALL DATE (5) MANUFACTURER (6) PROCEDURE NO. (7) TECHNICIAN (8) DATE				
(9) (10) (11) (12) (13) (14) (15)				

PROC. STEP NO. (1)	FUNCTION TESTED (2) NOV 29 1965	CALIBRATION DATA			CHECK ONE <input checked="" type="checkbox"/> DEVIATION <input type="checkbox"/> CORRECTION <input type="checkbox"/> ERROR <input type="checkbox"/> ACTUAL VALUE (6)	CALIBRATION TOLERANCES	
		NOMINAL (3)	MEASURED (4)	CORRECTED VALUE OF COLUMN (5)		LOWER LIMIT (7)	UPPER LIMIT (8)
	Test Cycles	N	R	AVER			
1	97.188	97.206	97.197				
2	97.180	97.196	97.188				
3	97.206	97.223	97.215				
4	97.208	97.225	97.217				
5	97.208	97.225	97.217				
6	97.207	97.225	97.216				
7	97.211	97.228	97.220				
8	97.220	97.238	97.229				
9	97.223	97.237	97.230				
10	97.222	97.238	97.229				
10 PT AVER 97.216 0.0332 DEVIATION							
Acceptable per chg 1126039 (Steps 1 and 2) H.C. Chandon 9 March 66							

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

10N 100° Th 100

DATE MAR - 7 1966

MAR - 7 1966

ASC 3-026-008

MANUFACTURER MODEL NO
HERONMETRICS 1126039

SERIAL NO.

PROCEDURE NO.

TECHNICIAN

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	<input checked="" type="checkbox"/> CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES					
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)				
		N	R	AVER							
1	98.358	98.508	98.433								
2	98.364	98.512	98.438								
3	98.370	98.517	98.444								
4	98.378	98.525	98.451								
5	98.376	98.524	98.450								
6	98.375	98.523	98.449								
7	98.385	98.532	98.460								
8	98.379	98.528	98.452								
9	98.382	98.526	98.454								
10	98.385	98.530	98.458								
		Av.	98.449	sc							

DK 0.027 sr
Acceptable per chg 1126039 (Steps 1 and 2)

H.C. Chandler 9 March 66

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ABC 3-029-003

MAR - 9 1966

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

ABC 3-026-008

DATE

MAR - 8 1966

(CONTINUED ON REVERSE SIDE)

CALIBRATION DATA SHEET

10% ice to LN_2

MAR - 8 1966

ABC 3-028-005

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	<input checked="" type="checkbox"/> CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES	
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)
		N	R	148.157			
1		98.070	98.210	98.140			
2		98.075	98.220	98.148			
3		98.087	98.229	98.158			
4		98.087	98.231	98.157			
5		98.089	98.235	98.162			
6		98.089	98.232	98.160			
7		98.086	98.229	98.158			
8		98.089	98.230	98.160			
9		98.090	98.235	98.162			
10		98.086	98.234	98.160			
		Av.		98.157 \pm 2			
		NR = 0.022 \pm 2					

$$\Delta R = 0.022 \text{ m}$$

Acceptable per drawing 1126037 (steps 1011 & 2)
11/20/06

(Steps 1 and 2)
H.C. Chamberlain 9 March 66

Enclosure 5
0700:1161

**ELEMENT CALIBRATION DATA
FOR 13 PRODUCTION TRANSDUCERS**

LINEAR DATA RECORD

AGCS 0711-36

GROUP CALIBRATION (SN 2, 5, 11, 12 & 19)

P/O T1-104A-200

MAR 15 1966

{CONTINUED ON THE NEXT PAGE}

LINEAR DATA RECORD

AGCS 0711-30

GROUP CALIBRATION ($SN_4, 22, 23, 24, 25$)

P10 T1-104A-200

DATE MAR 15 1980

MANUFACTURER		MODEL NO	SERIAL NO	PROCEDURE NO	TECHNICIAN
AC'IMETRICS	1126039	4		R J. 7A/308	
MANUFACTURER	MODEL NO	SERIAL NO	CALIBRATION DATE	MANUFACTURER	MODEL NO
ROH	162D	162	4/27/6		
LEA	8069B	1564785	2/17/7		
"	7559	1594791	8/3/6		
"	7563	1228751	4/27/6		
"	7835	1569152	9/3/6		
HAR	865B	1262	7/28/6		
EPA	100	702608	3/10/6		

CALIBRATION DATA

	STD °K	STD °C	$\frac{100}{K}$	RT -2	RATIO $\frac{RT}{98.264}$	RATIO $\frac{RT}{98.320}$
MAR - 9 1988						
ICE				98.264	1.000000	
LN ₂	77.519	-195.631	1.290001	123.128	1.253033	
ICE				98.264	1.000000	
CRYOSTAT	42.124	-231.673	2.373943	152.692	1.553896	
	37.785	-235.366	2.646552	159.900	1.627250	
	30.956	-242.195	3.230440	175.160	1.782546	
	26.471	-246.679	3.777661	189.488	1.928357	
	23.290	-249.860	4.293631	203.560	2.071563	
	19.295	-253.855	5.182689	227.928	2.319548	
	20.871	-252.279	4.791338	216.960	2.207930	
AMBIENT	295.440	22.290	0.338479	98.216	0.999512	
ICE				98.320		1.000000
60°C	331.390	58.240	0.3017592	98.524		1.002075
CO ₂	194.689	-78.461	0.5136390	100.916		1.026404
ICE				98.316		0.999959

Acceptable for drug 11260391 Sty 3) H.C. Chandalon 15 Mar 66

GROUP CALIBRATION (SN 2, 5, 11, 12 + 19)

LINEAR DATA RECORD

LINEAR
AGCS 0711-36

PLO T1-104A-200

MAR 15 1966

CALIBRATION DATA

	STD °K	STD °C	$\frac{100}{K}$	RT Ω	RATIO $\frac{RT}{98.816}$	
MAR - 1 1966						
ICE				96.816	1.000000	
MAR - 2 1966						
ICE				96.816	1.000000	
CO ₂	195.454	-77.676	0.511627	99.424	1.026938	
LN ₂	77.474	-195.676	1.270751	121.320	1.253099	
LN _e	27.070	-246.070	3.674127	183.840	1.898860	
MAR - 3 1966						
ICE				96.820	1.000041	
MAR - 7 1966						
ICE				96.840	1.000248	
CRYOSTAT	77.446	-195.704	1.271222	121.256	1.252438	
MAR - 8 1966						
CRYOSTAT	93.410	-179.740	1.070549	114.616	1.183854	
	88.200	-184.950	1.133786	116.844	1.206867	
	63.701	-209.449	1.569834	129.028	1.332714	
	48.065	-225.085	2.080515	142.640	1.473310	
	38.882	-234.268	2.571884	155.440	1.605520	
	31.360	-241.790	3.188776	171.120	1.767476	
	23.156	-249.994	4.318535	200.432	2.070236	
	19.346	-253.804	5.169027	223.632	2.307866	
MAR - 9 1966						
60°C	333.193	60.043	0.300126	97.080	1.002727	
ICE				96.840	1.000248	
Acceptable per Surge	1126039 (step 3)	N.C. Chamber	15 Mar 66			

(CONTINUED ON REVERSE SIDE)

Element

SIV 6 2004 10

LINEAR DATA RECORD

AGCS 071136

SIV 6 MUS 10

FEB 15 1986

Element

Group Classification

LINEAR DATA RECORD

AGCS 071136

CARTOONISTS AND THE CIVIL WAR

DATE FEB 15 1986

CALIBRATION DATA

	ST10 °K	ST 1 °C	100 %	AT V.L.	ST10 °T ST10, 016	
DEC 17 1965						
ICE		0		97.016	1.000000	
ICE				97.016	1.000000	
DEC 17 1965	29.436	-243.714	3.39725	176.198	1.815659	
CRYOSTAT	25.788	-247.162	3.84801	187.508	1.932753	
(22.429	-250.721	4.45855	203.352	2.096067	
)	18.727	-254.422	5.33942	227.304	2.342954	
)	16.302	-256.898	6.13436	250.040	2.577307	
DEC 18 1965						
(37.528	-235.622	2.66459	157.452	1.622949	
)	40.588	-232.562	2.46375	151.940	1.566133	
)	45.206	-227.944	2.21209	145.496	1.499711	
)	52.195	-220.955	1.91570	137.840	1.420797	
)	63.155	-209.995	1.58340	128.988	1.329554	
)	78.787	-194.363	1.269299	120.376	1.240785	
)	97.573	-175.577	1.024873	113.520	1.170116	
DEC 20 1965						
CRYOSTAT	122.404	-150.746	0.816167	107.868	1.111858	
ICE				97.052		
CO ₂	194.642	-78.508	0.513763	99.840	1.029109	
LN ₂	77.478	-195.652	1.27036	121.056	1.247794	
LNG	27.131	-246.019	3.685920	183.252	1.888534	
ICE				97.048		
DEC 21 1965						
AMBIENT	274.463	21.313		97.068	1.000639	
60°C	331.749	58.599	0.301432	97.156	1.001443	
ICE				97.052		
Acceptable per Aug 11/26/039 (Step 3)	11.0.01	...				9 Mar 66

Acceptable per Aug 11 26037 (Step 3) H.C. Ahern Co. 9 Mar 66

(CONTINUED ON REVERSE SIDE)

LINEAR DATA RECORD

AGCS 0711-36

GROUP C PRACTITIONERS

S/11 6 1100 13

FEB 15 1966

CALIBRATION DATA

	STD °K	STD °C	$\frac{100}{K}$	RT Ω	RATIO $\frac{RT}{96.624}$	RATIO $\frac{RT}{96.660}$
DEC 17 1965						
ICE				96.624		
ICE				96.624		
DEC 17 1965						
CRYOSTAT	29.436 - 243.714	3.31725	176.580	1.827496		
	25.988 - 247.162	3.84801	187.952	1.745190		
	22.427 - 250.721	4.45855	203.924	2.110490		
	18.729 - 254.422	5.33942	228.128	2.360987		
	16.302 - 256.848	6.13436	250.720	2.594386		
DEC 18 1965						
(CO ₂)	37.528 - 235.622	2.66487	157.628	1.631355		
	40.588 - 232.562	2.46375	151.998	1.572570		
	45.206 - 227.944	2.21209	145.440	1.505217		
	52.195 - 220.955	1.91590	137.728	1.425402		
	63.155 - 209.995	1.58340	128.832	1.333333		
	78.787 - 194.363	1.26724	120.152	1.243500		
	97.573 - 175.577	1.02487	113.288	1.172462		
DEC 20 1965						
CRYOSTAT	122.404 - 150.746	0.816967	107.594	1.113015	1.112596	
ICE				96.660		
CO ₂	194.642 - 78.508	0.513763	99.996	1.029724	1.029336	
N ₂	77.498 - 195.652	1.290360	120.760	1.251863	1.251392	
He	27.131 - 246.019	3.685820	183.400	1.898079	1.897365	
ICE				96.656		
DEC 21 1965						
AMBIENT	294.463	21.313		96.672	1.000497	1.000120
60°C	331.749	58.599	0.301432	96.752	1.001325	1.000948
100°C				96.660		

Accordable per diag 1135074 (Stg 1) No claim on 9 Mar. 86
(CONTINUED ON REVERSE SIDE)

GROUP COMMUNICATIONS (SN 2, 5, 11, 12 & 19)

LINEAR DATA RECORD

AGCS 071136

PL0 T1-100A-200

MAR 15 1966

CALIBRATION DATA

	STD °K	STD °C	$\frac{100}{K}$	R _T Ω	RATIO $\frac{R_T}{R_T}$ 97.199	
MAR - 1 1966						
ICE				97.199	1.000000	
MAR - 2 1966						
ICE				97.199	1.000000	
CO ₂	195.454	-77.696	0.511629	98.800	1.026759	
LN ₂	77.474	-195.676	1.290751	121.700	1.252070	
LNe	27.070	-246.080	3.694127	184.728	1.900513	
MAR - 3 1966						
ICE				97.204	1.000051	
MAR - 7 1966						
ICE				97.220	1.000216	
CRYOSTAT	77.446	-195.704	1.291222	121.708	1.252153	
MAR - 8 1966						
CRYOSTAT	93.410	-179.740	1.070549	115.060	1.183757	
	88.200	-184.950	1.133786	117.304	1.206893	
	63.701	-209.499	1.567834	129.608	1.333429	
	48.065	-225.085	2.080515	143.440	1.475735	
	38.882	-234.268	2.571884	156.344	1.608994	
	31.360	-241.790	3.188776	172.296	1.772611	
	23.156	-249.794	4.318535	202.052	2.078746	
	17.346	-253.804	5.169027	225.312	2.318049	
MAR - 9 1966						
60°C	333.193	60.043	0.300126	97.448	1.002562	
ICE				97.224	1.000257	

Acceptable for drug 1126039 (step 3) H. C. Chamberlain 15 Mar. 66

LINEAR DATA RECORD

AGCS 071136

GROUP CIVILIZATION (SN 2, 5, 11, 12+19)

P/0 T1-100A-200

MAR 15 1988

DATA

TECHNICIAN I
R 7/19/63

CALIBRATION DATA

	STD OK	STD OC	100/ K	RT SL	RATIO RT/ 98.044
MAR - 1 1966					
ICE				98.044	1.000000
MAR - 2 1966					
ICE				98.044	1.000000
CO ₂	195.454	- 77.696	0.511629	100.644	1.026519
LN ₂	77.474	- 195.676	1.290751	122.376	1.248174
LNe	27.070	- 246.080	3.694127	185.028	1.887194
MAR - 3 1966					
ICE				98.048	1.000041
MAR - 7 1966					
ICE				98.080	1.000367
CRYOSTAT	77.446	- 195.704	1.291222	122.244	1.246828
MAR - 8 1966					
CRYOSTAT	73.410	- 179.740	1.070349	115.644	1.179511
	88.200	- 184.750	1.133786	117.880	1.202317
	63.701	- 209.499	1.569834	130.116	1.327118
	48.065	- 225.085	2.080515	143.860	1.467300
	38.882	- 234.268	2.571884	156.596	1.597201
	31.360	- 241.790	3.188776	172.404	1.758435
	23.156	- 249.994	4.318535	201.892	2.059198
	19.346	- 253.804	5.169027	224.820	2.293052
MAR - 9 1966					
60 °C	333.173	60.043	0.300126	78.336	1.002978
ICE				78.080	1.000367

Acceptable per log 1126039 (stop 3) H.C. Chamberlain 15 Mar 66

(CONTINUED ON REVERSE SIDE)

LINEAR DATA RECORD
AGCS 0711-36

AGCS 0711-36

GROUP CALIBRATION (SN 2, 5, 11, 12 & 19)
P/L T-10-11-200

MAR 15 1966

CALIBRATION DATA

	STD °K	STD °C	$\frac{100}{K}$	RT -2	RATIO $\frac{RT}{97.763}$
17 - 1 1966					
ICE				97.763	1.000000
MAR - 2 1966					
ICE				97.763	1.000000
CO ₂	195.454	-77.696	0.511629	100.272	1.025664
LiI ₂	77.474	-195.676	1.290751	121.824	1.246116
LN _e	27.070	-246.080	3.694127	184.200	1.884148
31 MAR					
ICE				97.768	1.000051
JUN - 1 1966					
ICE				97.800	1.000378
CRYOSTAT	77.046	-195.704	1.291222	121.684	1.244684
8 JUN					
CRYOSTAT	93.390	-179.760	1.070778	115.088	1.177214
	88.561	-184.589	1.129165	117.356	1.200413
	63.806	-209.344	1.567250	129.516	1.324796
	48.076	-225.084	2.080339	143.160	1.464358
	38.882	-234.268	2.571884	155.728	1.592913
	31.363	-241.790	3.188776	171.440	1.753629
	23.156	-249.794	4.318535	200.712	2.053047
	19.396	-253.804	5.169027	223.600	2.287164
15 JUN					
60 °C	333.193	60.043	0.300126	98.020	1.002629
ICE				97.796	1.000338

Acceptable for day 1126039 (S.l.p. 5) H.C. Ohana Con 15 Mar 66

LINEAR DATA RECORD

AGCS 0711-36

GROUP CALIBRATION (SN 4, 22, 23, 24, 25)

P/I T1-104A-200

MAR 15 1966

MANUFACTUREP
MODEL NO.

MANUFACTURER	MODEL NO	SERIAL NO.	PROCEDURE NO	TECHNICIAN
ANIMETRICS	1126039	22		X

MANUFACTURER	MODEL NO	SERIAL NO.	RECALL DATE	EQUIPMENT MANUFACTURER	MODEL NO.	SERIAL NO.	RECALL DATE	MANUFACTUREP MODEL NO.
SAME AS S/N 4								

CALIBRATION DATA

	STD °K	STD °C	100/ K	R/T Ω	RATIO RT/ 98.564	RATIO RT/ 98.600
MAR - 9 1966						
ICE				98.564	1.000000	
LN ₂	77.519	-195.631	1.290001	124.244	1.260542	
ICE				98.564	1.000000	
CRYOSTAT	42.124	-231.673	2.373943	154.312	1.565603	
	37.785	-235.366	2.646552	161.616	1.639707	
	30.956	-242.195	3.230440	176.992	1.795708	
	26.471	-246.679	3.777661	191.548	1.943389	
	23.290	-249.260	4.293631	205.792	2.087904	
	19.295	-253.855	5.182689	230.568	2.339274	
	20.871	-252.279	4.791338	219.344	2.225398	
AMBIENT	295.440	22.290	0.338479	98.500		0.998986
ICE				98.600		1.000000
60°C	331.390	58.240	0.3017592	98.736		1.0013795
CO ₂	194.689	-78.461	0.5136390	101.580		1.030223
ICE				98.600		1.000000
Acceptable per Aug 1126039 (step 3) K.C. Charlton 15 March 66						

(CONTINUED ON REVERSE SIDE)

LINEAR DATA RECORD

AGCS 0711-36

GROUP CALIBRATION (SN 4, 22, 23, 24+25)
P% T1-104A-200

P/L T1-104A-200

DATE MAR 15 1966

CALIBRATION DATA

	STD. °K	STD. °C	$\frac{100}{K}$	RT °L	RATIO $\frac{RT}{96.520}$	RATIO $\frac{RT}{96.548}$
MAR - 9 1966						
ICE				96.520	1.000000	
LN ₂	77.519	-195.631	1.290001	121.684	1.260768	
ICE				96.520	1.000000	
CRYOSTAT	42.124	-231.673	2.373943	151.280	1.567412	
	37.785	-235.366	2.646552	158.444	1.641638	
	30.956	-242.195	3.230490	173.504	1.797675	
	26.471	-246.679	3.777661	187.844	1.946252	
	23.290	-249.860	4.293631	201.820	2.091057	
	19.295	-253.855	5.182689	226.388	2.345606	
	20.871	-252.279	4.791338	215.136	2.229024	
AMBIENT	295.440	22.290	0.338479	96.452	0.999295	
ICE				96.548		1.000000
60 °C	331.390	58.240	0.3017592	96.664		1.001197
CO ₂	194.629	-78.461	0.5136390	99.476		1.030323
ICE				96.552		1.000037

Acceptable per Aug 1126039 (step 3) H.C. Chandon 15 May 66

LINEAR DATA RECORD

AGCS 0711-36

GROUP CALIBRATION (SN 4, 22, 23, 24, & 25)
P/O T1-104A-200

MAR 15 1966

DATE

MANUFACTURER	MODEL NO	SERIAL NO	PROCEDURE NO	TECHNICIAN	MANUFACTURER	MODEL NO	SERIAL NO	PROCEDURE NO	TECHNICIAN
IRMETRICS	1126039	24		R	JTL	7A300			
MANUFACTURER	MODEL NO	SERIAL NO	CALIBRATION DATE	EQUIPMENT MANUFACTURER	MODEL NO	SERIAL NO	RECALL DATE	MANUFACTURER	MODEL NO
SAME AS	S/N 4								
CALIBRATION DATA									
	STD °K	STD °C	100/ K	RT Ω	RATIO				
MAR - 9 1966					RT 98.424				
ICE					98.424	1.000000			
LN ₂	77.519	-195.631	1.290001	123.840	123.840	1.258227			
ICE					98.424	1.000000			
CRYOSTAT	42.124	-231.673	2.373743	153.800	153.800	1.562623			
	37.785	-235.366	2.646552	161.040	161.040	1.636183			
	30.956	-242.195	3.230490	176.240	176.240	1.790616			
	26.471	-246.679	3.777661	190.716	190.716	1.937694			
	23.270	-249.860	4.293631	204.800	204.800	2.080788			
	19.295	-253.855	5.182689	229.632	229.632	2.333084			
	20.871	-252.279	4.791338	218.400	218.400	2.218966			
AMBIENT	295.440	22.290	0.338479	98.276	98.276	0.998494			
ICE					98.424	1.000000			
60°C	331.390	58.290	0.3017592	98.484	98.484	1.000607			
CO ₂	194.689	-78.461	0.5136390	101.304	101.304	1.029259			
ICE					98.428	1.000038			
Acceptable per day 1126039 (step 3) H.C. Chamberlain Mar 66									

(CONTINUED ON REVERSE SIDE)

LINEAR DATA RECORD
AGCS 071-36

AGCS 0711-36

GROUP CALIBRATION ISN 4, 22, 23, 24, + 25)

P/0 T1-104A-200

DATE MAR 15 1966

CALIBRATION DATA

	STD °K	STD °C	100/ K	RT Ω	RATIO RT / 98.096	RATIO RT / 98.192
MAR - 9 1986						
ICE				98.096	1.000000	
LN ₂	77.519	-195.631	1.290001	123.244	1.256349	
ICE				98.096	1.000000	
CRYOSTAT	42.124	-231.673	2.373943	152.568	1.555278	
	37.785	-235.366	2.646552	159.620	1.627166	
	30.956	-242.195	3.230490	174.516	1.779016	
	26.471	-246.679	3.777661	188.648	1.923078	
	23.290	-249.860	4.293631	203.304	2.072481	
	19.295	-253.855	5.182689	226.524	2.309186	
	20.871	-252.279	4.791338	215.920	2.201088	
AMBIENT	295.440	22.290	0.338479	98.094	0.999461	
ICE				98.192		1.000000
60 °C	331.390	58.240	0.301668	98.276		1.000843
CO ₂	194.689	78.461	0.5136390	101.090		1.028991
ICE				98.188		0.999947

Accesible per day 1126039 (step 3) H.C. Chamberlain 15 Mar 66

**Enclosure 6
0700:1161**

AEROMETRICS

TEST PROCEDURE 7905-007

AEROMETRICS TEST PROCEDURE 7905-007

ACCEPTANCE TEST PROCEDURE FOR

MODEL TI 104A-200

TEMPERATURE TRANSDUCER

CONTRACT NO. NAS 8-11862

28 MARCH 1966

APPROVALS:

H.C. Chandler
Project Engineer

J.W. Spangler
Quality Control Manager

APPROVED FOR:

NASA Representative

ACCEPTANCE TEST PROCEDURE FOR
TEMPERATURE TRANSDUCER
MODEL T1 104A-200

1. PURPOSE

To demonstrate compliance with the requirements of NASA Contract NAS 8-11862

2. TEST PROCEDURE

Step 1. ELECTRICAL CONTINUITY TEST

Measure and record the electrical resistance at ambient temperature ($72 \pm 5^{\circ}\text{F}$), between the blue and black terminal; red and blue terminal; and tan and black terminal. The resistance limits shall be as follows:

Blue to black - Between 95 and 105 ohms

Red to Blue - Between 6 and 10 ohms

Tan to Black - Between 9 and 14 ohms

Step 2. INSULATION TEST

Measure and record the insulation resistance between the red terminal and the housing at ambient temperature ($72 \pm 5^{\circ}\text{F}$). The resistance shall be greater than 10 Megohms when measured with 50 VDC potential. All surfaces are to be dry and free from moisture.

Step 3. CALIBRATION

Using the circuit shown in Figure 1, calibrate each transducer in fixed baths of ice/water, carbon dioxide, liquid nitrogen, and liquid neon. Calibrate each transducer in an adjustable temperature bath at $60 \pm 5^{\circ}\text{C}$.

Step 4. RESPONSE TEST

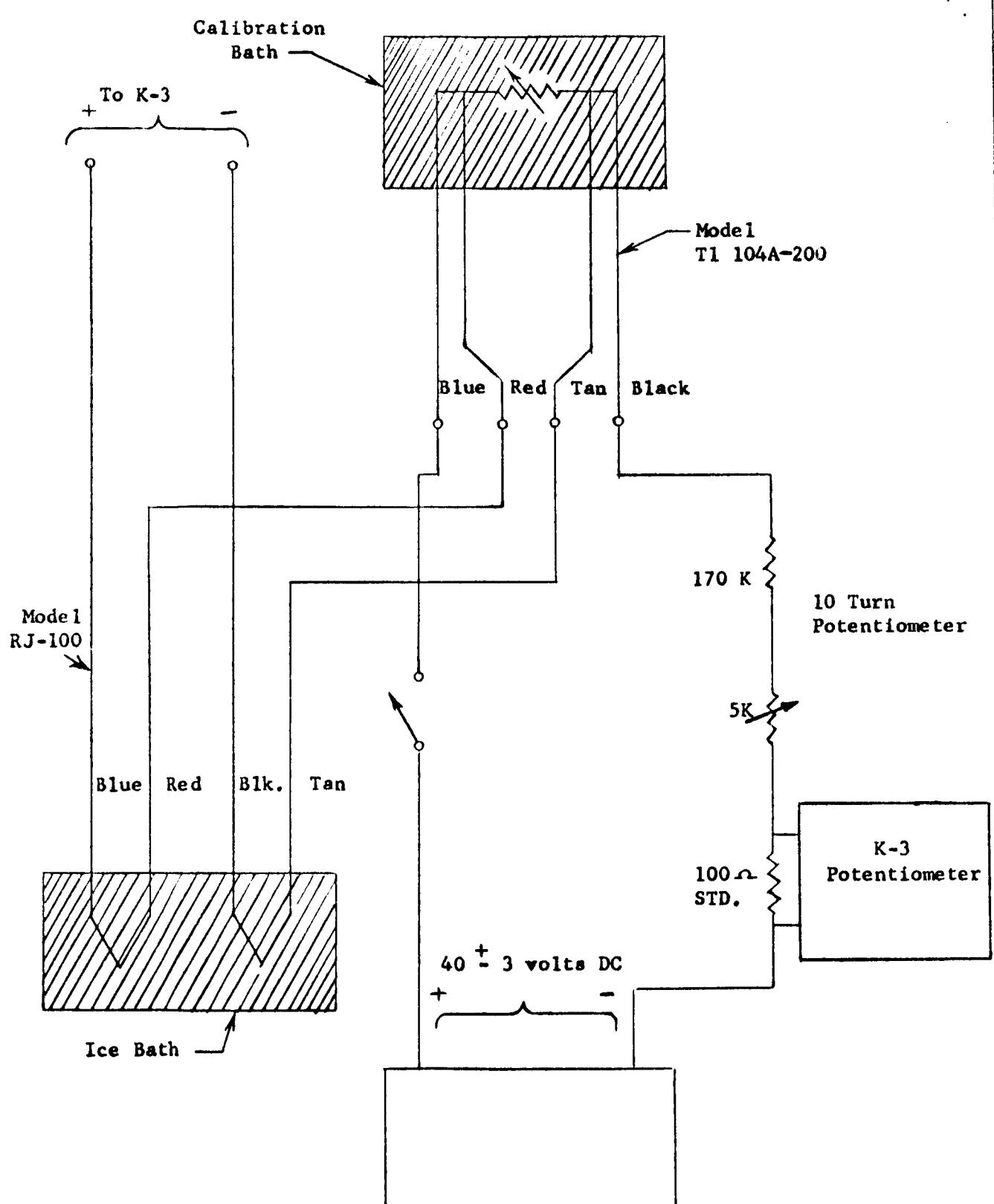
Using the setup per Figure 2 and circuit per Figure 3, measure and record the one time constant (63%) response for a change in the output signal for temperature changes from -196°C to -246°C and -246°C to -196°C . The average of two cycles shall not exceed 0.25 seconds.

Step 5. POST ELECTRICAL CONTINUITY TEST

Repeat Step 1.

Step 6. POST INSULATION TEST

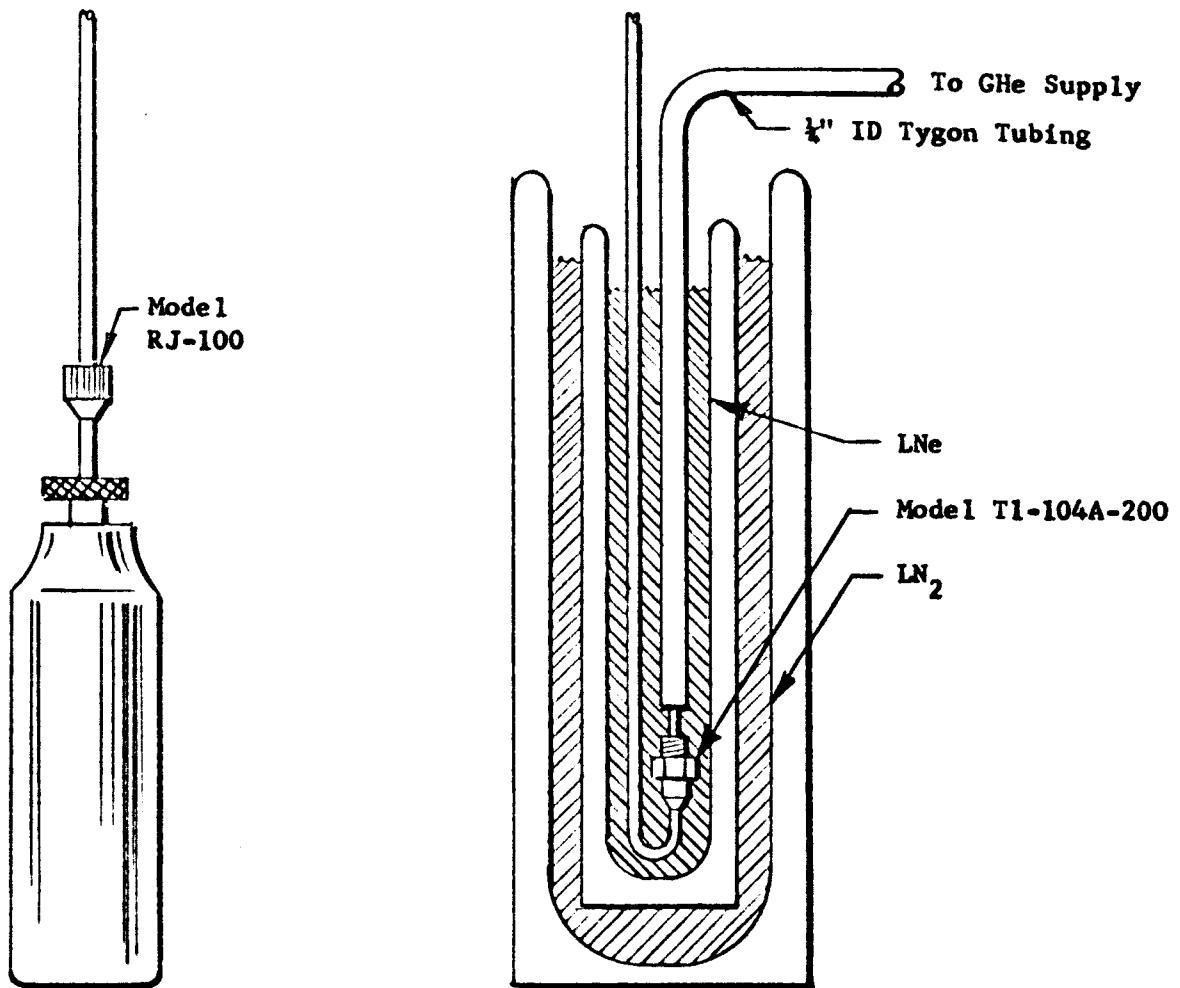
Repeat Step 2.



NOTE: Adjust the 5K 10 turn potentiometer
for a 23.0 mv drop across the 100 Ω . Std.

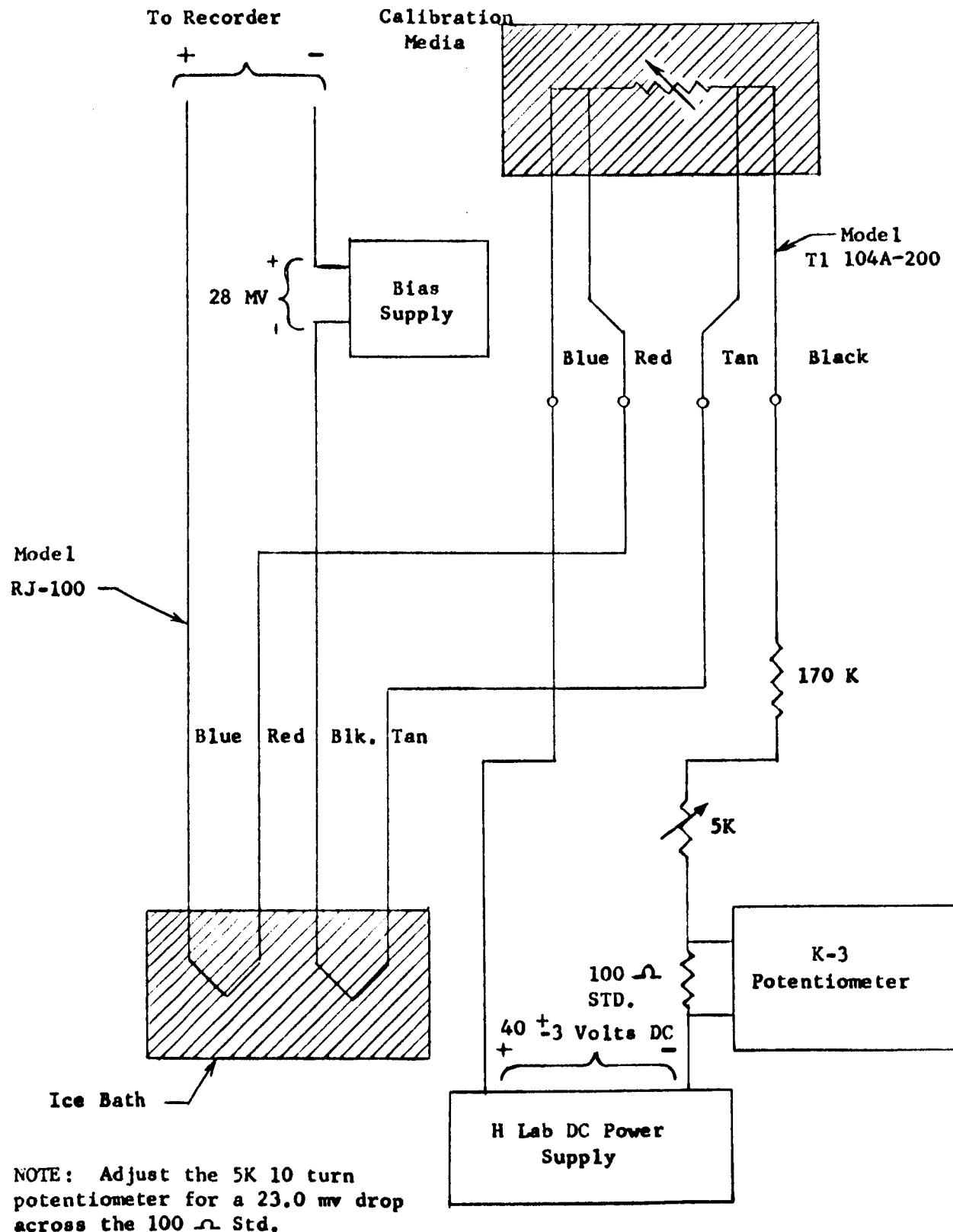
FIGURE - 1

To Instrumentation



RESPONSE TEST SETUP

FIGURE - 2



RESPONSE TEST CIRCUIT

FIGURE - 3

Enclosure 7
0700:1161

**ACCEPTANCE TEST DATA
FOR 13 PRODUCTION TRANSDUCERS**

PAGE 1 of 11

CALIBRATION DATA SHEET

ABC 1-029-001

DATE 23 MARCH 66

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES	
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)
STEP 1.	ELECTRICAL					TEST	
		SN	BLUE BLACK	RED BLUE	TAN BLACK		
		95 min	6 min	9 min		SPECIFICATION	
		105 max	10 max	14 max		LIMITS	
2	97.2 Ω	8.0 Ω	10.6 Ω				
4	101.2	7.9	10.4				
5	95.9	7.8	10.6				
6	98.8	8.0	10.5				
9	97.8	7.9	10.7				
10	97.4	7.9	10.5				
11	96.0	7.7	10.6				
12	97.8	7.5	10.5				
19	97.4	8.0	10.6				
22	99.3	8.4	10.7				
23	97.2	7.8	10.6				
24	98.0	7.9	10.6				
25	97.6	7.8	10.6				
All	reading are acceptable					N.O. Chaudhury	
						23 March 1966	

All reading are acceptable N.O. Charnley
23 March 1966

N. O. Charaloy
23 March 1966

CALIBRATION DATA SHEET

ABC 3-026-005

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES	
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)
		STEP 2.	INSULATION TEST				
		5V	RED CASE				
			10 Meg min				
		2	>10,000 Meg ohms				
		4	>10,000				
		5	>10,000				
		6	>10,000				
		9	>10,000				
		10	>10,000				
		11	>10,000				
		12	>10,000				
		19	>10,000				
		22	>10,000				
		23	>10,000				
		24	>10,000				
		25	>10,000				
		All readings are acceptable				H. L. Chauhan 23 May 1966	

STEP 3 CALIBRATION

Page 3 of 11

CALIBRATION DATA SHEET

MANUFACTURER	MODEL NO.	SERIAL NO.	PROCEDURE NO.	DATE
ZEROMETRICS	71-104A-200	As Notes	ATP 7905-007	23 MARCH 1966
LEA	7553	154479/39451964		
EPA	100	104408/10441964		
LEA	7553	1208515/120861966		

CALIBRATION DATA SHEET

MANUFACTURER	MODEL NO.	PROCEDURE NO.	DATE	TECHNICIAN	CALIBRATION DATA		CALIBRATION TOLERANCES	
					FUNCTION TESTED	PROC. STEP NO.	FUNCTION TESTED	PROC. STEP NO.
ZEROMETRICS	71-104A-200	As Notes	ATP 7905-007	R	MEASURED	(a)	MEASURED	(a)
LEA	7553	154479/39451964			COLUMN OF VALUES	(b)	COLUMN OF VALUES	(b)
EPA	100	104408/10441964			ACTUAL VALUE	(c)	ACTUAL VALUE	(c)
LEA	7553	1208515/120861966			LOWER LIMIT	(d)	LOWER LIMIT	(d)
ZEROMETRICS	71-104A-200	As Notes	ATP 7905-007	R	UPPER LIMIT	(e)	UPPER LIMIT	(e)
LEA	7553	154479/39451964			DEVIATION	(f)	DEVIATION	(f)
EPA	100	104408/10441964			CHECK ONE DEVIATION	(g)	CHECK ONE DEVIATION	(g)
LEA	7553	1208515/120861966			CONNECTION	(h)	CONNECTION	(h)
ZEROMETRICS	71-104A-200	As Notes	ATP 7905-007	R	BRIDGE	(i)	BRIDGE	(i)
LEA	7553	154479/39451964			ACTUAL VALUE	(j)	ACTUAL VALUE	(j)
EPA	100	104408/10441964			UPPER LIMIT	(k)	UPPER LIMIT	(k)
LEA	7553	1208515/120861966			LOWER LIMIT	(l)	LOWER LIMIT	(l)

 $\frac{1}{23} = 4.547826086$

STEP 3 CALIBRATION

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CALIBRATION DATA SHEET

MANUFACTURER			TECHNICIAN			PROCEDURE NO.			DATE		
TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.
SOMETRICS	TI-104A-200	As Noted	ATP	7905-007	(D)						
2CH	1620	169	29 March 66								
<i>All other components same as page 2 of 11</i>											

CALIBRATION DATA SHEET

CALIBRATION DATA			CALIBRATION TOLERANCES			CALIBRATION DATA			CALIBRATION TOLERANCES		
TEST NO.	FUNCTION TESTED	READING OR VALUE	TEST NO.	FUNCTION TESTED	READING OR VALUE	TEST NO.	FUNCTION TESTED	READING OR VALUE	TEST NO.	FUNCTION TESTED	READING OR VALUE
1	N 4.8167	79.5356°C	8.664	8.650	36.652	36.599	8.709	8.045	0.059	±5%	✓ 0.53
2	R 4.8084	-320.304°F	✓	N 4.8163	79.5215°C	8.663	8.649	37.607	37.549	8.710	0.047
4	R 4.8077	-220.312°F	✓	N 4.8164	79.4180°C	8.664	8.649	36.217	36.162	8.710	0.047
5	N 4.8160	79.593°C	✓	R 4.8073	79.4215°C	8.647	8.634	36.872	36.812	8.708	0.061
6	N 4.8222	-195.934°C	✓	R 4.8130	-220.222°F	8.647	8.634	36.872	36.812	8.708	0.061
7	N 4.8164	79.5210°C	✓	N 4.8167	79.5210°C	8.668	8.653	36.783	36.723	8.710	0.042
9	R 4.8077	-320.312°F	✓	R 4.8074	-320.304°F	8.662	8.647	36.663	36.606	8.709	0.057
10	N 4.8167	79.5218°C	✓	R 4.8084	-320.304°F	8.662	8.647	36.663	36.606	8.709	0.039
11	R 4.8073	79.4233°C	✓	N 4.8163	79.4170°C	8.671	8.652	36.110	36.060	8.710	0.057
12	R 4.8163	79.5218°C	✓	R 4.8070	-320.319°F	8.666	8.650	36.706	36.658	8.710	0.044
13	R 4.8072	-320.317°F	✓	R 4.8160	79.593°C	8.663	8.649	36.584	36.530	8.710	0.047
14	N 4.8160	79.518°C	✓	R 4.8075	-320.317°F	8.663	8.649	36.584	36.530	8.710	0.044
22	N 4.8167	79.5230°C	✓	R 4.8084	-320.304°F	8.665	8.651	37.352	37.300	8.709	0.058
23	N 4.8167	79.5260°C	✓	N 4.8167	79.5290°C	8.632	8.632	36.733	36.673	8.709	0.062
24	N 4.8163	79.5230°C	✓	R 4.8070	-320.317°F	8.667	8.653	36.887	36.833	8.710	0.057
25	R 4.8222	-195.934°C	✓	N 4.8130	-220.220°F	8.647	8.635	36.622	36.563	8.708	0.061
	R 4.8130	-220.220°F									

All 100% of all tests failed 11/11/66 - 24/11/66

MANUFACTURER			TECHNICIAN			PROCEDURE NO.			DATE		
TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.
SOMETRICS	TI-104A-200	As Noted	ATP	7905-007	(D)						
2CH	1620	169	29 March 66								
<i>all other components same as page 2 of 11</i>											

MANUFACTURER			TECHNICIAN			PROCEDURE NO.			DATE		
TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.	TEST NO.
SOMETRICS	TI-104A-200	As Noted	ATP	7905-007	(D)						
2CH	1620	169	29 March 66								
<i>all other components same as page 2 of 11</i>											

(CONTINUED ON OTHER SIDE)

STEP 3 CALIBRATION SHEET 5-0-11

CALIBRATION DATA SHEET

ITEM	TESTER	TESTER NO.	TESTER NO.	PROCEDURE NO.	PROCEDURE NO.	TESTER NO.	TESTER NO.	TESTER NO.	TESTER NO.
1	162D	169	29 March 66	ATP 7905-007	R				
2	All other equipment			Calibration factor	0.000092				
3	Same as page 6 of H								
4									

CALIBRATION DATA SHEET

PROC. STEP NO.	FUNCTION TESTED	MEASURED	CALIBRATION TOLERANCE	CALIBRATION DATA				PROC. STEP NO.	FUNCTION TESTED	MEASURED	CALIBRATION TOLERANCE	
				ACTUAL VALUE	COLUMN NO.	CHECK ONE	CONNECTION					
1	LIVE POINT Mueller	9.605	±0.000092	9.605	1	✓	STANDARD	1	Aerodynamics	9.665	±0.000092	✓
2	N	9.605	±0.000092	9.605	2	✓	STD - No load	2	TCL(mV)	9.665	±0.000092	✓
3	N	9.605	±0.000092	9.605	3	✓	STD - No load	3	TCL(mV)	9.665	±0.000092	✓
4	N	9.605	±0.000092	9.605	4	✓	STD - No load	4	TCL(mV)	9.665	±0.000092	✓
5	N	9.605	±0.000092	9.605	5	✓	STD - No load	5	TCL(mV)	9.665	±0.000092	✓
6	N	9.605	±0.000092	9.605	6	✓	STD - No load	6	TCL(mV)	9.665	±0.000092	✓
7	N	9.605	±0.000092	9.605	7	✓	STD - No load	7	TCL(mV)	9.665	±0.000092	✓
8	N	9.605	±0.000092	9.605	8	✓	STD - No load	8	TCL(mV)	9.665	±0.000092	✓
9	N	9.605	±0.000092	9.605	9	✓	STD - No load	9	TCL(mV)	9.665	±0.000092	✓
10	N	9.605	±0.000092	9.605	10	✓	STD - No load	10	TCL(mV)	9.665	±0.000092	✓
11	N	9.605	±0.000092	9.605	11	✓	STD - No load	11	TCL(mV)	9.665	±0.000092	✓
12	N	9.605	±0.000092	9.605	12	✓	STD - No load	12	TCL(mV)	9.665	±0.000092	✓
13	N	9.605	±0.000092	9.605	13	✓	STD - No load	13	TCL(mV)	9.665	±0.000092	✓
14	N	9.605	±0.000092	9.605	14	✓	STD - No load	14	TCL(mV)	9.665	±0.000092	✓
15	N	9.605	±0.000092	9.605	15	✓	STD - No load	15	TCL(mV)	9.665	±0.000092	✓
16	N	9.605	±0.000092	9.605	16	✓	STD - No load	16	TCL(mV)	9.665	±0.000092	✓
17	N	9.605	±0.000092	9.605	17	✓	STD - No load	17	TCL(mV)	9.665	±0.000092	✓
18	N	9.605	±0.000092	9.605	18	✓	STD - No load	18	TCL(mV)	9.665	±0.000092	✓
19	N	9.605	±0.000092	9.605	19	✓	STD - No load	19	TCL(mV)	9.665	±0.000092	✓
20	N	9.605	±0.000092	9.605	20	✓	STD - No load	20	TCL(mV)	9.665	±0.000092	✓
21	N	9.605	±0.000092	9.605	21	✓	STD - No load	21	TCL(mV)	9.665	±0.000092	✓
22	N	9.605	±0.000092	9.605	22	✓	STD - No load	22	TCL(mV)	9.665	±0.000092	✓
23	N	9.605	±0.000092	9.605	23	✓	STD - No load	23	TCL(mV)	9.665	±0.000092	✓
24	N	9.605	±0.000092	9.605	24	✓	STD - No load	24	TCL(mV)	9.665	±0.000092	✓
25	N	9.605	±0.000092	9.605	25	✓	STD - No load	25	TCL(mV)	9.665	±0.000092	✓
26	N	9.605	±0.000092	9.605	26	✓	STD - No load	26	TCL(mV)	9.665	±0.000092	✓
27	N	9.605	±0.000092	9.605	27	✓	STD - No load	27	TCL(mV)	9.665	±0.000092	✓
28	N	9.605	±0.000092	9.605	28	✓	STD - No load	28	TCL(mV)	9.665	±0.000092	✓
29	N	9.605	±0.000092	9.605	29	✓	STD - No load	29	TCL(mV)	9.665	±0.000092	✓
30	N	9.605	±0.000092	9.605	30	✓	STD - No load	30	TCL(mV)	9.665	±0.000092	✓
31	N	9.605	±0.000092	9.605	31	✓	STD - No load	31	TCL(mV)	9.665	±0.000092	✓
32	N	9.605	±0.000092	9.605	32	✓	STD - No load	32	TCL(mV)	9.665	±0.000092	✓
33	N	9.605	±0.000092	9.605	33	✓	STD - No load	33	TCL(mV)	9.665	±0.000092	✓
34	N	9.605	±0.000092	9.605	34	✓	STD - No load	34	TCL(mV)	9.665	±0.000092	✓
35	N	9.605	±0.000092	9.605	35	✓	STD - No load	35	TCL(mV)	9.665	±0.000092	✓
36	N	9.605	±0.000092	9.605	36	✓	STD - No load	36	TCL(mV)	9.665	±0.000092	✓
37	N	9.605	±0.000092	9.605	37	✓	STD - No load	37	TCL(mV)	9.665	±0.000092	✓
38	N	9.605	±0.000092	9.605	38	✓	STD - No load	38	TCL(mV)	9.665	±0.000092	✓
39	N	9.605	±0.000092	9.605	39	✓	STD - No load	39	TCL(mV)	9.665	±0.000092	✓
40	N	9.605	±0.000092	9.605	40	✓	STD - No load	40	TCL(mV)	9.665	±0.000092	✓
41	N	9.605	±0.000092	9.605	41	✓	STD - No load	41	TCL(mV)	9.665	±0.000092	✓
42	N	9.605	±0.000092	9.605	42	✓	STD - No load	42	TCL(mV)	9.665	±0.000092	✓
43	N	9.605	±0.000092	9.605	43	✓	STD - No load	43	TCL(mV)	9.665	±0.000092	✓
44	N	9.605	±0.000092	9.605	44	✓	STD - No load	44	TCL(mV)	9.665	±0.000092	✓
45	N	9.605	±0.000092	9.605	45	✓	STD - No load	45	TCL(mV)	9.665	±0.000092	✓
46	N	9.605	±0.000092	9.605	46	✓	STD - No load	46	TCL(mV)	9.665	±0.000092	✓
47	N	9.605	±0.000092	9.605	47	✓	STD - No load	47	TCL(mV)	9.665	±0.000092	✓
48	N	9.605	±0.000092	9.605	48	✓	STD - No load	48	TCL(mV)	9.665	±0.000092	✓
49	N	9.605	±0.000092	9.605	49	✓	STD - No load	49	TCL(mV)	9.665	±0.000092	✓
50	N	9.605	±0.000092	9.605	50	✓	STD - No load	50	TCL(mV)	9.665	±0.000092	✓
51	N	9.605	±0.000092	9.605	51	✓	STD - No load	51	TCL(mV)	9.665	±0.000092	✓
52	N	9.605	±0.000092	9.605	52	✓	STD - No load	52	TCL(mV)	9.665	±0.000092	✓
53	N	9.605	±0.000092	9.605	53	✓	STD - No load	53	TCL(mV)	9.665	±0.000092	✓
54	N	9.605	±0.000092	9.605	54	✓	STD - No load	54	TCL(mV)	9.665	±0.000092	✓
55	N	9.605	±0.000092	9.605	55	✓	STD - No load	55	TCL(mV)	9.665	±0.000092	✓
56	N	9.605	±0.000092	9.605	56	✓	STD - No load	56	TCL(mV)	9.665	±0.000092	✓
57	N	9.605	±0.000092	9.605	57	✓	STD - No load	57	TCL(mV)	9.665	±0.000092	✓
58	N	9.605	±0.000092	9.605	58	✓	STD - No load	58	TCL(mV)	9.665	±0.000092	✓
59	N	9.605	±0.000092	9.605	59	✓	STD - No load	59	TCL(mV)	9.665	±0.000092	✓
60	N	9.605	±0.000092	9.605	60	✓	STD - No load	60	TCL(mV)	9.665	±0.000092	✓
61	N	9.605	±0.000092	9.605	61	✓	STD - No load	61	TCL(mV)	9.665	±0.000092	✓
62	N	9.605	±0.000092	9.605	62	✓	STD - No load	62	TCL(mV)	9.665	±0.000092	✓
63	N	9.605	±0.000092	9.605	63	✓	STD - No load	63	TCL(mV)	9.665	±0.000092	✓
64	N	9.605	±0.000092	9.605	64	✓	STD - No load	64	TCL(mV)	9.665	±0.000092	✓
65	N	9.605	±0.000092	9.605	65	✓	STD - No load	65	TCL(mV)	9.665	±0.000092	✓
66	N	9.605	±0.000092	9.605	66	✓	STD - No load	66	TCL(mV)	9.665	±0.000092	✓
67	N	9.605	±0.000092	9.605	67	✓	STD - No load	67	TCL(mV)	9.665	±0.000092	✓
68	N	9.605	±0.000092	9.605	68	✓	STD - No load	68	TCL(mV)	9.665	±0.000092	✓
69	N	9.605	±0.000092	9.605	69	✓	STD - No load	69	TCL(mV)	9.665	±0.000092	✓
70	N	9.605	±0.000092	9.605	70	✓	STD - No load	70	TCL(mV)	9.665	±0.000092	✓
71	N	9.605	±0.000092	9.605	71	✓	STD - No load	71	TCL(mV)	9.665	±0.000092	✓
72	N	9.605	±0.000092	9.605	72	✓	STD - No load	72	TCL(mV)	9.665	±0.000092	✓
73	N	9.605	±0.000092	9.605	73	✓	STD - No load	73	TCL(mV)	9.665	±0.000092	✓
74	N	9.605	±0.000092	9.605	74	✓	STD - No load	74	TCL(mV)	9.665	±0.000092	✓
75	N	9.605	±0.000092	9.605	75	✓	STD - No load	75	TCL(mV)	9.665	±0.000092	✓
76	N	9.605	±0.000092	9.605	76	✓	STD - No load	76	TCL(mV)	9.665	±0.000092	✓
77	N	9.605	±0.000092	9.605	77	✓	STD - No load	77	TCL(mV)	9.665	±0.000092	✓
78	N	9.605	±0.000092	9.605	78	✓	STD - No load	78	TCL(mV)	9.665	±0.000092	✓
79	N	9.605	±0.000092	9.605	79	✓	STD - No load	79	TCL(mV)	9.665	±0.000092	✓
80	N	9.605	±0.000092	9.605	80	✓	STD - No load	80	TCL(mV)	9.665	±0.000092	✓
81	N	9.605	±0.000092	9.605	81	✓	STD - No load	81	TCL(mV)	9.665	±0.000092	✓
82	N	9.605	±0.000092	9.605	82	✓	STD - No load	82	TCL(mV)	9.665	±0.000092	✓
83	N	9.605	±0.000092	9.605	83	✓	STD - No load	83	TCL(mV)	9.665	±0.000092	✓
84	N	9.605	±0.000092	9.605	84	✓	STD - No load	84	TCL(mV)	9.665	±0.000092	✓
85	N	9.605	±0.000092	9.605	85	✓	STD - No load	85	TCL(mV)	9.665	±0.000092	✓
86	N	9.605	±0.000092	9.605	86	✓	STD - No load	86	TCL(mV)	9.665	±0.000092	✓
87	N	9.605	±0.000092	9.605								

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CALIBRATION DATA SHEET

CALIBRATION DATA SHEET

MANUFACTURER		MODEL NO.	Serial No.	PROCEDURE NO.	PROCEDURE NO.	DATE	TECHNICIAN
MANUFACTURER		MODEL NO.	Serial No.	PROCEDURE NO.	PROCEDURE NO.	DATE	TECHNICIAN
CALIBRATION EQUIPMENT							
TEST INSTRUMENTS							
LEA 6163	1619833	17Aug967					
LEA 6069 8	1564785	17Aug967					
LEA 9835	1569152	3Aug966					
LEA 7559	1544791	3Aug966					
LEA 100	202608	10Aug966	-0.0119	-0.0001FF			
LEA 7553	1206515	17Aug966					

MANUFACTURER		MODEL NO.	Serial No.	PROCEDURE NO.	PROCEDURE NO.	DATE	TECHNICIAN
MANUFACTURER		MODEL NO.	Serial No.	PROCEDURE NO.	PROCEDURE NO.	DATE	TECHNICIAN
CALIBRATION EQUIPMENT							
TEST INSTRUMENTS							
LEA 6163	1619833	17Aug967					
LEA 6069 8	1564785	17Aug967					
LEA 9835	1569152	3Aug966					
LEA 7559	1544791	3Aug966					
LEA 100	202608	10Aug966	-0.0119	-0.0001FF			
LEA 7553	1206515	17Aug966					

MANUFACTURER		MODEL NO.	Serial No.	PROCEDURE NO.	PROCEDURE NO.	DATE	TECHNICIAN
MANUFACTURER		MODEL NO.	Serial No.	PROCEDURE NO.	PROCEDURE NO.	DATE	TECHNICIAN
CALIBRATION EQUIPMENT							
TEST INSTRUMENTS							
LEA 6163	1619833	17Aug967					
LEA 6069 8	1564785	17Aug967					
LEA 9835	1569152	3Aug966					
LEA 7559	1544791	3Aug966					
LEA 100	202608	10Aug966	-0.0119	-0.0001FF			
LEA 7553	1206515	17Aug966					

(Continued on reverse side)

STEP 3 CALIBRATION PISTOL 90+11

CALIBRATION DATA SHEET

TEST NO	TEST DATE	TEST NO	TEST DATE	TEST NO	TEST DATE
LEA 3163	1552859	1902 ACC			
7 off other equipment same as page 6 of 11		COMP - 0.000050			

CALIBRATION DATA SHEET

TEST NO	FUNCTION TESTED	CALIBRATION DATA		CALIBRATION TO STANDARD		TEST NO	FUNCTION TESTED	CALIBRATION DATA		CALIBRATION TO STANDARD	
		MEASUREMENT OR VALUE	REFERENCE	MEASUREMENT	REFERENCE			MEASUREMENT OR VALUE	REFERENCE	MEASUREMENT	REFERENCE
1.	AU	17.4637	194.87305	4.192	27.953	27.356	4.210	0.012	0.018	1.513242	✓
2.	R	17.4637	-108.96305	4.192	27.237	4.208	4.210	-0.007	0.003	1.513116	✓
3.	AU	17.4637	194.87305	4.192	27.170	27.133	4.210	0.010	0.016	1.513242	✓
4.	R	17.4637	-108.96305	4.192	27.050	4.225	4.210	0.010	0.016	1.513242	✓
5.	AU	17.4637	194.87305	4.192	26.975	26.743	4.192	-0.005	0.005	1.513242	✓
6.	R	17.4637	-108.96305	4.192	26.898	26.782	4.192	-0.010	0.005	1.513242	✓
7.	AU	17.4637	194.87305	4.192	26.822	26.743	4.192	-0.005	0.005	1.513242	✓
8.	R	17.4637	-108.96305	4.192	26.743	26.675	4.192	-0.005	0.005	1.513242	✓
9.	AU	17.4637	194.87305	4.192	26.675	26.637	4.192	-0.005	0.005	1.513242	✓
10.	R	17.4637	-108.96305	4.192	26.637	26.599	4.192	-0.005	0.005	1.513242	✓
11.	AU	17.4637	194.87305	4.192	26.599	26.561	4.192	-0.005	0.005	1.513242	✓
12.	R	17.4637	-108.96305	4.192	26.561	26.524	4.192	-0.005	0.005	1.513242	✓
13.	AU	17.4637	194.87305	4.192	26.524	26.486	4.192	-0.005	0.005	1.513242	✓
14.	R	17.4637	-108.96305	4.192	26.486	26.448	4.192	-0.005	0.005	1.513242	✓
15.	AU	17.4637	194.87305	4.192	26.448	26.410	4.192	-0.005	0.005	1.513242	✓
16.	R	17.4637	-108.96305	4.192	26.410	26.372	4.192	-0.005	0.005	1.513242	✓
17.	AU	17.4637	194.87305	4.192	26.372	26.334	4.192	-0.005	0.005	1.513242	✓
18.	R	17.4637	-108.96305	4.192	26.334	26.296	4.192	-0.005	0.005	1.513242	✓
19.	AU	17.4637	194.87305	4.192	26.296	26.258	4.192	-0.005	0.005	1.513242	✓
20.	R	17.4637	-108.96305	4.192	26.258	26.220	4.192	-0.005	0.005	1.513242	✓
21.	AU	17.4637	194.87305	4.192	26.220	26.182	4.192	-0.005	0.005	1.513242	✓
22.	R	17.4637	-108.96305	4.192	26.182	26.144	4.192	-0.005	0.005	1.513242	✓
23.	AU	17.4637	194.87305	4.192	26.144	26.106	4.192	-0.005	0.005	1.513242	✓
24.	R	17.4637	-108.96305	4.192	26.106	26.068	4.192	-0.005	0.005	1.513242	✓
25.	AU	17.4637	194.87305	4.192	26.068	26.030	4.192	-0.005	0.005	1.513242	✓
26.	R	17.4637	-108.96305	4.192	26.030	25.992	4.192	-0.005	0.005	1.513242	✓
27.	AU	17.4637	194.87305	4.192	25.992	25.954	4.192	-0.005	0.005	1.513242	✓
28.	R	17.4637	-108.96305	4.192	25.954	25.916	4.192	-0.005	0.005	1.513242	✓
29.	AU	17.4637	194.87305	4.192	25.916	25.878	4.192	-0.005	0.005	1.513242	✓
30.	R	17.4637	-108.96305	4.192	25.878	25.840	4.192	-0.005	0.005	1.513242	✓
31.	AU	17.4637	194.87305	4.192	25.840	25.802	4.192	-0.005	0.005	1.513242	✓
32.	R	17.4637	-108.96305	4.192	25.802	25.764	4.192	-0.005	0.005	1.513242	✓
33.	AU	17.4637	194.87305	4.192	25.764	25.726	4.192	-0.005	0.005	1.513242	✓
34.	R	17.4637	-108.96305	4.192	25.726	25.688	4.192	-0.005	0.005	1.513242	✓
35.	AU	17.4637	194.87305	4.192	25.688	25.650	4.192	-0.005	0.005	1.513242	✓
36.	R	17.4637	-108.96305	4.192	25.650	25.612	4.192	-0.005	0.005	1.513242	✓
37.	AU	17.4637	194.87305	4.192	25.612	25.574	4.192	-0.005	0.005	1.513242	✓
38.	R	17.4637	-108.96305	4.192	25.574	25.536	4.192	-0.005	0.005	1.513242	✓
39.	AU	17.4637	194.87305	4.192	25.536	25.498	4.192	-0.005	0.005	1.513242	✓
40.	R	17.4637	-108.96305	4.192	25.498	25.460	4.192	-0.005	0.005	1.513242	✓
41.	AU	17.4637	194.87305	4.192	25.460	25.422	4.192	-0.005	0.005	1.513242	✓
42.	R	17.4637	-108.96305	4.192	25.422	25.384	4.192	-0.005	0.005	1.513242	✓
43.	AU	17.4637	194.87305	4.192	25.384	25.346	4.192	-0.005	0.005	1.513242	✓
44.	R	17.4637	-108.96305	4.192	25.346	25.308	4.192	-0.005	0.005	1.513242	✓
45.	AU	17.4637	194.87305	4.192	25.308	25.270	4.192	-0.005	0.005	1.513242	✓
46.	R	17.4637	-108.96305	4.192	25.270	25.232	4.192	-0.005	0.005	1.513242	✓
47.	AU	17.4637	194.87305	4.192	25.232	25.194	4.192	-0.005	0.005	1.513242	✓
48.	R	17.4637	-108.96305	4.192	25.194	25.156	4.192	-0.005	0.005	1.513242	✓
49.	AU	17.4637	194.87305	4.192	25.156	25.118	4.192	-0.005	0.005	1.513242	✓
50.	R	17.4637	-108.96305	4.192	25.118	25.080	4.192	-0.005	0.005	1.513242	✓
51.	AU	17.4637	194.87305	4.192	25.080	25.042	4.192	-0.005	0.005	1.513242	✓
52.	R	17.4637	-108.96305	4.192	25.042	25.004	4.192	-0.005	0.005	1.513242	✓
53.	AU	17.4637	194.87305	4.192	25.004	24.966	4.192	-0.005	0.005	1.513242	✓
54.	R	17.4637	-108.96305	4.192	24.966	24.928	4.192	-0.005	0.005	1.513242	✓
55.	AU	17.4637	194.87305	4.192	24.928	24.890	4.192	-0.005	0.005	1.513242	✓
56.	R	17.4637	-108.96305	4.192	24.890	24.852	4.192	-0.005	0.005	1.513242	✓
57.	AU	17.4637	194.87305	4.192	24.852	24.814	4.192	-0.005	0.005	1.513242	✓
58.	R	17.4637	-108.96305	4.192	24.814	24.776	4.192	-0.005	0.005	1.513242	✓
59.	AU	17.4637	194.87305	4.192	24.776	24.738	4.192	-0.005	0.005	1.513242	✓
60.	R	17.4637	-108.96305	4.192	24.738	24.699	4.192	-0.005	0.005	1.513242	✓
61.	AU	17.4637	194.87305	4.192	24.699	24.661	4.192	-0.005	0.005	1.513242	✓
62.	R	17.4637	-108.96305	4.192	24.661	24.623	4.192	-0.005	0.005	1.513242	✓
63.	AU	17.4637	194.87305	4.192	24.623	24.585	4.192	-0.005	0.005	1.513242	✓
64.	R	17.4637	-108.96305	4.192	24.585	24.547	4.192	-0.005	0.005	1.513242	✓
65.	AU	17.4637	194.87305	4.192	24.547	24.509	4.192	-0.005	0.005	1.513242	✓
66.	R	17.4637	-108.96305	4.192	24.509	24.471	4.192	-0.005	0.005	1.513242	✓
67.	AU	17.4637	194.87305	4.192	24.471	24.433	4.192	-0.005	0.005	1.513242	✓
68.	R	17.4637	-108.96305	4.192	24.433	24.395	4.192	-0.005	0.005	1.513242	✓
69.	AU	17.4637	194.87305	4.192	24.395	24.357	4.192	-0.005	0.005	1.513242	✓
70.	R	17.4637	-108.96305	4.192	24.357	24.319	4.192	-0.005	0.005	1.513242	✓
71.	AU	17.4637	194.87305	4.192	24.319	24.281	4.192	-0.005	0.005	1.513242	✓
72.	R	17.4637	-108.96305	4.192	24.281	24.243	4.192	-0.005	0.005	1.513242	✓
73.	AU	17.4637	194.87305	4.192	24.243	24.205	4.192	-0.005	0.005	1.513242	✓
74.	R	17.4637	-108.96305	4.192	24.205	24.167	4.192	-0.005	0.005	1.513242	✓
75.	AU	17.4637	194.87305	4.192	24.167	24.129	4.192	-0.005	0.005	1.513242	✓
76.	R	17.4637	-108.96305	4.192	24.129	24.091	4.192	-0.005	0.005	1.513242	✓
77.	AU	17.4637	194.87305	4.192	24.091	24.053	4.192	-0.005	0.005	1.513242	✓
78.	R	17.4637	-108.96305	4.192	24.053	23.915	4.192	-0.005	0.005	1.513242	✓
79.	AU	17.4637	194.87305	4.192	23.915	23.877	4.192	-0.005	0.005	1.513242	✓
80.	R	17.4637	-108.96305	4.192	23.877	23.839	4.192	-0.005	0.005	1.513242	✓
81.	AU	17.4637	194.87305	4.192	23.839	23.791	4.192	-0.005	0.005	1.513242	✓
82.	R	17.4637	-108.96305	4.192	23.791	23.753	4.192	-0.005	0.005	1.513242	✓
83.	AU	17.4637	194.87305	4.192	23.753	23.715	4.192	-0.005	0.005	1.513242	✓
84.	R	17.4637	-108.96305	4.192	23.715	23.677	4.192	-0.005	0.005		

STEP 4 Response Test PAGE 9 of 11

CALIBRATION DATA SHEET

DATE 25 MARCH 1966

CALIBRATION DATA

PROC. STEP NO.	FUNCTION TESTED	READING OR VALUE		CORRECTED COLUMN	CHECK ONE		CALIBRATION TOLERANCES	
		NOMINAL	MEASURED		DEVIATION	CORRECTION	LOWER LIMIT	UPPER LIMIT
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
	Re-prise Test - LN2			to LN ₂ (ITC, 63%) sec				
3N	1.57	2.12	3.0				Holding	
2	0.18	0.17	0.14				0.163	
4	0.20	0.20	0.25				0.218	
5	0.18	0.16	0.15				0.163	
6	0.15	0.18	0.22				0.218	
O 9	0.18	0.18	0.15				0.170	
10	0.20	0.23	0.20				0.210	
11	0.17	0.20	0.18				0.181	
12	0.21	0.21	0.19				0.203	
19	0.17	0.16	0.20				0.178	
22	0.15	0.20	0.19				0.173	
23	0.17	0.18	0.17				0.173	
24	0.16	0.18	0.21				0.183	
25	0.13	0.16	0.14				0.143	

All readings are acceptable N.O. Chandler
25 March 1966

av. 0.1695

STEP 5 Post CONTINUITY TEST PAGE 10 of 11

CALIBRATION DATA SHEET

DATE 25 MARCH 1966

MANUFACTURER		MODEL NO.	SERIAL NO.	PROCEDURE NO.		TECHNICIAN		MANUFACTURER MODEL NO.
OXYMETRICS		TI-104A-200	As Noted	ATP 7905-007		R	LPI	
MANUFACTURER		MODEL NO.	SERIAL NO.	CALIBRATION EQUIPMENT				
LEA	4232-B	1573937	23 Aug 1966					
LEA	9B35-B	1546482	27 Oct 1966					
CALIBRATION DATA								
PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE <input checked="" type="checkbox"/> DEVIATION <input type="checkbox"/> CORRECTION <input type="checkbox"/> ERROR <input type="checkbox"/> ACTUAL VALUE (6)	CALIBRATION TOLERANCES		
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)	
STEP 5	STANDARD 100% CONTINUITY TEST	100% BLACK	100% BLACK	6 MIN.	7 MAX.	100% BLACK	100% BLACK	
		100% MAX.	100% MAX.	10 MAX.	14 MAX.	100% MAX.	100% MAX.	
1	97.3	8.2	10.6					
2	101.4	8.0	10.5					
3	96.2	8.2	10.5					
4	99.2	8.2	10.5					
5	98.1	8.1	10.7					
6	98.0	8.0	10.5					
7	96.5	8.0	10.6					
8	97.9	8.1	10.7					
9	97.6	8.1	10.7					
10	99.5	8.2	10.6					
11	97.4	8.2	10.6					
12	98.0	8.1	10.6					
13	98.2	8.2	10.5					
All readings are acceptable						H.C. Chandalor 25 March 1966		

(CONTINUED ON REVERSE SIDE)

STEP 6 POST INSULATION TEST PAGE 11 of 11

CALIBRATION DATA SHEET

MEC 2-028-028

DATE 25 MARCH 1966

CALIBRATION DATA

PROC. STEP NO. (1)	FUNCTION TESTED (2)	READING OR VALUE		CORRECTED VALUE OF COLUMN (5)	CHECK ONE DEVIATION CORRECTION ERROR ACTUAL VALUE (6)	CALIBRATION TOLERANCES	
		NOMINAL (3)	MEASURED (4)			LOWER LIMIT (7)	UPPER LIMIT (8)
	STEP 6		INSULATION TEST RED CASE				
	S/N		10 MEG MIN.				
	2	> 10,000	MEG OHMS				
	4	> 10,000					
	5	> 10,000					
	6	> 10,000					
	9	> 10,000					
	10	> 10,000					
	11	> 10,000					
	12	> 10,000					
	19	> 10,000					
	22	> 10,000					
	23	> 10,000					
	24	> 10,000					
	25	> 10,000					
	All readings are acceptable.		H.C. Chambon				
			25 March 1966				

All readings are acceptable

H.C. Chameleon
25 March 1966

Enclosure 8
0700:1161

AEROMETRICS

CHROMEL-CONSTANTAN

THERMOCOUPLE EMF vs TEMPERATURE TABLE

AEROMETRICS
 Chromel-Constantan
 Thermocouple EMF vs Temperature Table

Temperature °C	mv. Out		Temperature °C	mv. Out	
	No Load	100K Load		No Load	100K Load
-273	9.787	9.763			
-272	9.786	9.762			
-271	9.785	9.761			
-270	9.785	9.761	-240	9.554	9.532
-269	9.784	9.760	-239	9.541	9.519
-268	9.781	9.757	-238	9.527	9.506
-267	9.778	9.754	-237	9.514	9.493
-266	9.775	9.751	-236	9.500	9.479
-265	9.771	9.747	-235	9.486	9.465
-264	9.767	9.743	-234	9.472	9.451
-263	9.763	9.739	-233	9.458	9.437
-262	9.758	9.735	-232	9.443	9.422
-261	9.752	9.729	-231	9.427	9.406
-260	9.747	9.724	-230	9.410	9.390
-259	9.741	9.712	-229	9.394	9.374
-258	9.735	9.712	-228	9.377	9.357
-257	9.728	9.705	-227	9.359	9.339
-256	9.721	9.692	-226	9.342	9.322
-255	9.713	9.690	-225	9.322	9.303
-254	9.705	9.672	-224	9.304	9.285
-253	9.694	9.673	-223	9.285	9.266
-252	9.683	9.655	-222	9.265	9.247
-251	9.677	9.655	-221	9.246	9.228
-250	9.668	9.546	-220	9.227	9.209
-249	9.658	9.536	-219	9.207	9.189
-248	9.646	9.524	-218	9.187	9.169
-247	9.637	9.515	-217	9.166	9.149
-246	9.626	9.503	-216	9.145	9.128
-245	9.614	9.592	-215	9.124	9.107
-244	9.602	9.580	-214	9.103	9.086
-243	9.590	9.568	-213	9.081	9.064
-242	9.578	9.556	-212	9.059	9.042
-241	9.566	9.544	-211	9.036	9.020

Temperature °C	mv. Out		Temperature °C	mv. Out	
	No Load	100K Load		No Load	100K Load
-210	8.013	8.007	-170	7.905	7.892
-209	8.020	8.074	-169	7.873	7.860
-208	8.067	8.050	-168	7.841	7.828
-207	8.044	8.027	-167	7.808	7.796
-206	8.020	8.003	-166	7.777	7.764
-205	8.006	8.000	-165	7.744	7.731
-204	8.072	8.056	-164	7.711	7.699
-203	8.048	8.032	-163	7.677	7.665
-202	8.023	8.007	-162	7.644	7.632
-201	8.700	8.703	-161	7.610	7.598
-200	8.773	8.757	-160	7.577	7.565
-199	8.747	8.732	-159	7.543	7.531
-198	8.721	8.706	-158	7.509	7.497
-197	8.695	8.680	-157	7.474	7.463
-196	8.669	8.654	-156	7.440	7.428
-195	8.642	8.627	-155	7.405	7.393
-194	8.615	8.600	-154	7.370	7.358
-193	8.588	8.573	-153	7.354	7.343
-192	8.560	8.545	-152	7.298	7.287
-191	8.532	8.469	-151	7.264	7.252
-190	8.505	8.491	-150	7.227	7.215
-189	8.477	8.463	-149	7.191	7.180
-188	8.449	8.435	-148	7.155	7.144
-187	8.420	8.401	-147	7.119	7.107
-186	8.390	8.377	-146	7.083	7.072
-185	8.362	8.343	-145	7.046	7.035
-184	8.332	8.313	-144	7.009	6.998
-183	8.302	8.283	-143	6.972	6.961
-182	8.272	8.250	-142	6.935	6.924
-181	8.242	8.220	-141	6.898	6.887
-180	8.213	8.199	-140	6.860	6.849
-179	8.183	8.169	-139	6.822	6.811
-178	8.152	8.139	-138	6.784	6.774
-177	8.121	8.103	-137	6.746	6.735
-176	8.091	8.078	-136	6.708	6.697
-175	8.061	8.043	-135	6.669	6.659
-174	8.030	8.017	-134	6.630	6.620
-173	7.998	7.985	-133	6.591	6.581
-172	7.967	7.954	-132	6.552	6.541
-171	7.936	7.924	-131	6.512	6.502

Temperature °C	mv. Out		Temperature °C	mv. Out	
	No Load	100K Load		No Load	100K Load
-130	6.472	6.462	- 90	4.741	4.734
-129	6.433	6.423	- 89	4.694	4.687
-128	6.393	6.383	- 88	4.643	4.644
-127	6.354	6.344	- 87	4.601	4.594
-126	6.313	6.303	- 86	4.553	4.546
-125	6.273	6.263	- 85	4.506	4.499
-124	6.232	6.223	- 84	4.458	4.452
-123	6.191	6.182	- 83	4.411	4.404
-122	6.150	6.140	- 82	4.363	4.356
-121	6.104	6.094	- 81	4.315	4.308
-120	6.067	6.058	- 80	4.267	4.261
-119	6.025	6.016	- 79	4.217	4.211
-118	5.983	5.974	- 78	4.171	4.164
-117	5.942	5.932	- 77	4.123	4.117
-116	5.900	5.891	- 76	4.075	4.168
-115	5.857	5.848	- 75	4.026	4.020
-114	5.814	5.805	- 74	3.977	3.971
-113	5.771	5.763	- 73	3.929	3.923
-112	5.729	5.720	- 72	3.879	3.873
-111	5.686	5.677	- 71	3.830	3.824
-110	5.642	5.633	- 70	3.781	3.775
-109	5.599	5.591	- 69	3.731	3.725
-108	5.556	5.547	- 68	3.681	3.676
-107	5.512	5.503	- 67	3.632	3.626
-106	5.468	5.459	- 66	3.582	3.577
-105	5.423	5.415	- 65	3.533	3.527
-104	5.379	5.371	- 64	3.482	3.476
-103	5.335	5.326	- 63	3.431	3.426
-102	5.290	5.282	- 62	3.381	3.375
-101	5.245	5.237	- 61	3.330	3.325
-100	5.200	5.192	- 60	3.279	3.274
- 99	5.155	5.147	- 59	3.229	3.224
- 98	5.110	5.102	- 58	3.178	3.173
- 97	5.064	5.056	- 57	3.126	3.121
- 96	5.018	5.010	- 56	3.076	3.071
- 95	4.972	4.965	- 55	3.024	3.019
- 94	4.926	4.919	- 54	2.972	2.968
- 93	4.881	4.873	- 53	2.921	2.916
- 92	4.835	4.827	- 52	2.869	2.865
- 91	4.788	4.781	- 51	2.787	2.783

Temperature °C	mv. Out		Temperature °C	mv. Out	
	No Load	100K Load		No Load	100K Load
-50	2.765	2.761	-10	0.578	0.577
-49	2.713	2.709	-9	0.521	0.521
-48	2.660	2.656	-8	0.462	0.462
-47	2.608	2.604	-7	0.405	0.405
-46	2.555	2.551	-6	0.347	0.347
-45	2.503	2.499	-5	0.288	0.288
-44	2.450	2.446	-4	0.230	0.230
-43	2.396	2.393	-3	0.171	0.171
-42	2.344	2.340	-2	0.113	0.113
-41	2.290	2.287	-1	0.055	0.055
-40	2.237	2.234	0	0.004	0.004
-39	2.184	2.180	1	-0.053	-0.053
-38	2.130	2.127	2	-0.110	-0.110
-37	2.076	2.073	3	-0.168	-0.168
-36	2.023	2.020	4	-0.226	-0.226
-35	1.968	1.965	5	-0.282	-0.282
-34	1.915	1.912	6	-0.341	-0.341
-33	1.860	1.857	7	-0.399	-0.399
-32	1.805	1.803	8	-0.457	-0.457
-31	1.751	1.748	9	-0.516	-0.516
-30	1.696	1.693	10	-0.574	-0.574
-29	1.641	1.639	11	-0.632	-0.632
-28	1.587	1.584	12	-0.691	-0.691
-27	1.532	1.530	13	-0.749	-0.750
-26	1.476	1.472	14	-0.808	-0.808
-25	1.421	1.417	15	-0.867	-0.868
-24	1.366	1.364	16	-0.926	-0.927
-23	1.310	1.309	17	-0.985	-0.986
-22	1.255	1.253	18	-1.043	-1.044
-21	1.199	1.197	19	-1.102	-1.103
-20	1.143	1.141	20	-1.162	-1.163
-19	1.087	1.085	21	-1.221	-1.222
-18	1.031	1.030	22	-1.281	-1.282
-17	0.975	0.973	23	-1.340	-1.342
-16	0.918	0.917	24	-1.399	-1.401
-15	0.862	0.861	25	-1.459	-1.460
-14	0.806	0.805	26	-1.518	-1.520
-13	0.749	0.748	27	-1.579	-1.580
-12	0.692	0.691	28	-1.640	-1.641
-11	0.636	0.635	29	-1.700	-1.701

Temperature °C	mv. Out	
	No Load	100Ω Load
30	-1.760	-1.761
31	-1.820	-1.822
32	-1.880	-1.882
33	-1.941	-1.942
34	-2.002	-2.003
35	-2.061	-2.062
36	-2.122	-2.123
37	-2.183	-2.184
38	-2.245	-2.246
39	-2.306	-2.307
40	-2.367	-2.368
41	-2.366	-2.367
42	-2.420	-2.422
43	-2.551	-2.553
44	-2.612	-2.613
45	-2.674	-2.675
46	-2.736	-2.737
47	-2.798	-2.799
48	-2.859	-2.861
49	-2.921	-2.923
50	-2.983	-2.985
51	-3.046	-3.047
52	-3.108	-3.109
53	-3.171	-3.172
54	-3.232	-3.234
55	-3.295	-3.296
56	-3.356	-3.359
57	-3.421	-3.422
58	-3.483	-3.485
59	-3.546	-3.548
60	-3.609	-3.611

Enclosure 9
0700:1161

**CALIBRATION DATA SHEETS
FOR 13 PRODUCTION TRANSDUCERS**

CALIBRATION DATA SHEET
SN 2

13 April 1966

CALIBRATION DATA SHEET

SECTION 4

CALIBRATION DATA SHEET

S.P. Chandon	5 April 1966	Collected full name	Transfered Collection Date

Transferred Collection Date	Transferred Collection Date	Transferred Collection Date
Calculated with Harry		

then: when deviation from calculated range

Temp.		NO LOAD						100 K LOAD						
Current	Voltage	Element		TC		Transformer Output		Element		TC		Transformer Output		
		$R_o = 98.3478$	$E_o = 0.123mV$	(1)	(2)	(1)	(2)	(3)	(4)	(3)	(4)	(5)	(6)	
$T_c = 0^\circ C$	$100^\circ C$	$\frac{E_o}{R_o}$	R_T	mV	mV	mV	mV	mV	mV	mV	mV	mV	mV	
C_{12235}														
16.3072	-251.8486	B4346	2.596644	253.374	58.736	9.727		16.022	63.485	254.724	58.587	9.704	+0.008	
18.727	-254.4324	5.339442	2.349629	3.31.068	53.150	9.708			62.880	230.535	53.023	9.685	-62.716	
20.152	-253	4.942728	2.244496	220.742	50.770	9.696			60.488	220.255	50.659	9.63	-60.340	
22.4298	-251.721	4.48555	2.103675	206.891	47.585	9.674			57.281	206.464	47.487	9.652	-57.147	
25.9888	-247.162	3.849801	1.738765	10.673	43.855	9.638			53.515	180.310	43.771	9.615	-53.394	
LNE2	27.131	-246.015	3.685820	1.897676	186.338	42.973	9.626		52.621	186.489	42.892	9.603	-52.503	
LNE2	27.135	-246.015	3.685277	1.897618	186.823	42.969	9.626		52.677	186.489	42.889	9.603	-52.500	
29.436	-242.714	3.39725	1.820610	179.053	41.182	9.598		0.016	50.794	178.733	41.109	9.577	-0.002	
37.528	-235.621	2.644578	1.626320	159.950	36.788	9.495		-0.004	46.279	157.694	36.730	9.474	-0.017	
40.5888	-233.512	2.443755	1.570029	154.409	35.574	9.451		-0.011	44.954	154.172	35.440	9.430	-0.024	
45.2046	-222.944	2.242209	1.502987	147.816	33.998	9.376		-0.023	43.351	147.598	33.948	9.355	-0.037	
52.195	-220.955	1.91590	1.6233785	140.018	32.204	9.245		-0.039	41.410	139.822	32.159	9.227	-0.051	
63.155	-209.955	1.583440	1.332019	131.001	30.130	9.013		-0.066	39.077	130.830	30.091	8.997	-0.078	
LNE2	72.448	-195.652	1.19036	1.351493	123.081	28.309	8.659		-0.100	36.868	122.930	28.274	8.645	-0.111
LNE2	72.448	-195.679	1.290826	1.251654	123.078	28.312	8.660		-0.100	36.872	122.947	28.278	8.645	-0.111
78.787	-194.303	1.269244	1.2428659	122.331	28.136	8.625			36.661	122.182	28.102	8.610	-0.111	
83.150	-150	1.022495	1.224469	120.424	27.657	8.525			36.102	120.280	27.664	8.491	-0.110	
97.373	-75.577	1.0259873	1.172209	115.333	26.527	8.078			34.505	115.200	26.496	8.065	-0.109	
122.4046	-150	75.746	0.816967	113.632	109.523	25.170			32.345	109.403	25.1163	7.257	-0.104	
CO2	194.642	-78.508	0.573763	113.02036	101.322	23.299	4.194		27.393	101.200	23.276	4.188	-0.096	
CO2	194.837	-78.313	0.573142	109.94162	101.294	22.218	4.185	-0.100	27.393	101.192	23.274	4.178	-0.094	
11e	—	—	—	1.00000	98.34778	22.620	—	—	22.620	98.252	22.598	—	+0.008	
11e	—	—	—	1.00000	98.34778	22.620	—	—	22.620	98.252	22.598	—	+0.008	
10e8	294.463	21.313	—	1.00064	98.413	22.635	-1.240	0.012	21.407	98.317	22.613	-1.241	0.022	
56.762	—	1.001413	98.406	22.652	-3.342	19.309	+0.031	19.340	98.310	22.611	-3.344	19.347		
58.599	—	1.001152	98.490	22.653	-3.521			19.163	98.394	22.631	-3.523	19.155		
60	—	1.001480	98.493	22.653	-3.609			19.075	98.397	22.631	-3.611	19.067		
Element - $I_c R_o$ (er/k)		- 22.619994 (er/k)						↓						

CALIBRATION DATA SHEET

H.C.Chamberlain

CALIBRATION DATA SHEET
SN 10

N.C. Chander
6 April 1966

Temp.	Inverse Temp. $10^3/K$	No Load						100K Load						
		Element R_t/R_0	R_t	TC	Transistor Output	Element Transistor Output	Corrected Transistor Output	Element Transistor Output	Corrected Transistor Output	Transistor Output	Transistor Output	Transistor Output	Transistor Output	
K	C	$100/C_{22315}$												
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	
11.302	-258.848	6.13436	2.594286	251.474	57.840	9.727	0.195	67.762	250.934	57.715	9.704	0.236	67.655	
18.727	-254.422	5.339472	2.354987	228.850	52.636	9.708		62.539	228.327	52.515	9.685		62.436	
21.156	-253.475	4.97425	2.272249	320.249	50.656	9.696		60.547	319.766	50.546	9.673		60.451	
22.429	-252.721	4.45855	2.110490	204.570	47.051	9.674		56.920	204.151	46.955	9.652		56.843	
25.965	-257.162	3.84861	1.91540	188.547	43.366	9.638		53.199	188.191	43.284	9.615		53.135	
LN _c 27.131	-264.015	3.685820	1.897365	183.912	42.301	9.626		52.122	183.574	42.222	9.603		52.061	
LN _c 27.134	-264.016	3.685823	1.697168	183.912	42.298	9.626	51.924	+0.195	52.119	193.564	42.220	9.603	52.059	
LN _c	29.436	-243.716	3.397250	1.827996	177.139	40.742	9.598	0.190	50.530	176.826	40.670	9.577	0.228	50.475
37.528	-225.622	2.664659	1.631355	158.127	36.370	9.495	0.173	46.038	157.878	36.312	9.474	0.204	45.990	
40.558	-222.562	2.46375	1.572350	152.429	35.059	9.451	0.167	44.677	152.198	35.006	9.430	0.195	44.631	
45.206	-222.944	2.21209	1.505217	145.901	33.557	9.326	0.158	43.091	145.688	33.508	9.355	0.181	43.044	
52.195	-220.955	1.91370	1.425302	138.164	31.778	9.245	0.143	41.166	139.974	31.734	9.227	0.160	41.121	
63.155	-209.995	1.58346	1.333333	129.240	29.725	9.013	0.121	38.888	29.073	29.687	8.997	0.127	38.811	
77.498	-195.652	1.294616	1.251392	121.297	22.898	B.659	0.093	36.650	121.150	22.864	B.645	0.085	36.594	
LN _c	77.427	-162.723	1.29155	1.251632	121.340	22.602	C.662	36.570	+0.093	36.663	121.193	22.624	+0.085	36.666
78.787	-194.363	1.226944	1.242350	120.532	27.723	B.625	0.091	36.439	120.386	27.689	B.610	0.084	36.383	
E _c /150	-146	1.202645	1.224140	118.656	27.251	8.575	0.069	35.885	118.515	27.255	8.491	0.083	35.932	
9.753	-175.577	1.021823	1.172362	113.647	26.139	B.028	0.083	34.300	113.518	26.109	B.065	0.076	34.250	
122.404	-150.746	0.816947	1.111259	107.844	24.804	7.255	0.079	32.130	107.728	24.777	7.237	0.065	32.079	
CO _c	194.642	-78.308	0.513263	1.020336	99.774	22.948	4.194	0.039	27.181	99.674	22.925	4.188	0.032	27.145
CB _c	194.612	-78.308	0.513262	1.020324	99.756	22.946	4.185	0.039	27.170	99.666	22.913	4.178	0.032	27.135
LG _c	—	—	—	1.00000	96.930	22.294	—	—	22.294	96.836	22.272	—	0.006	22.266
LG _c	—	—	—	1.00000	96.930	22.294	—	22.294	96.836	22.272	—	22.272	0.006	22.264
A _c /8	294.443	21.313	—	1.00020	96.942	22.297	-1.240	0.060	21.119	96.011	22.083	-1.241	0.045	20.887
	56.752	—	—	1.00044	97.016	23.314	-3.3467	18.6497	10.164	97.011	96.924	22.223	-3.468	18.955
331.749	58.579	—	—	1.000896	97.022	22.315	-3.521	—	18.958	96.928	22.293	-3.523	18.900	
LG _c	60	—	—	1.000974	97.015	22.316	-3.609	—	18.871	96.931	22.294	-3.611	18.813	

$$\begin{aligned} (v) &= I_c R_T = I_c R_0 (R_T/R_0) \\ (v) &= (1) + (2) + (3) \\ (v) &= (5) + (10) \\ (v) &= (5) + (100K) \end{aligned}$$

$$(v) = (1) (0.23m)$$

$$(v) = (1.24(13) + (15))$$

CALIBRATION DATA SHEET

SN 12

H.C. Chamberlain

Temp.	Inverse Temp. 100/K or 100/R ₀	No LOAD												100K LOAD															
		Element $R_0 = 97.3043$				TC Temperature Coefficient of Resist.				Element Resistor Value				TC Temperature Coefficient of Resist.				Element Resistor Value				TC Temperature Coefficient of Resist.				Element Resistor Value			
K	C	R_T/R_0	R_T	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	mv	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(23)	(24)	(25)	(26)	(27)	(28)		
19.343	-253.804	5.163027	2.38352	223.124	51.319	9.703			0.205	61.227	222.628	51.204	9.680			0.193	61.077												
24.155	-253	4.962286	2.232342	217.655	50.019	9.696				59.950	217.132	49.940	9.673				0.183	59.906											
23.156	-245.984	4.318535	2.059198	200.359	46.085	9.668				55.958	199.969	45.993	9.646				0.173	55.832											
24.646	-246.080	3.659127	1.887194	183.632	42.235	9.627				53.067	183.295	42.158	9.604				0.163	51.955											
LNG	27.739	-34.01	3.164734	1.884691	183.399	42.182	9.626		0.205	52.013	183.064	42.105	9.603				0.153	51.906											
31.360	-241.790	3.188776	1.750455	171.104	39.354	9.575		0.196	49.125	170.872	39.287	9.553				0.185	49.025												
38.882	-234.248	2.571884	1.597201	155.414	35.745	9.476		0.181	45.402	155.173	35.690	9.455				0.172	45.317												
48.065	-225.085	2.080515	1.467300	142.775	32.638	9.324		0.163	42.325	142.571	32.791	9.305				0.156	42.252												
63.201	-203.449	1.5616834	1.377118	129.134	29.701	9.000		0.131	38.832	128.968	29.663	8.984				0.128	38.775												
64.774	-195.672	1.290737	1.249714	124.452	27.934	8.660		0.105	36.699	121.305	27.900	8.645				0.106	36.657												
65.774	-195.722	1.291662	1.246642	121.475	27.939	8.662		0.105	36.706	121.328	27.905	8.647				0.106	36.658												
83.150	-150	1.202045	1.121231	116.938	27.356	8.505		0.102	35.963	118.797	27.323	8.491				0.104	35.918												
88.200	-184.950	1.133782	1.1202317	116.911	26.908	8.361		0.099	35.368	116.854	26.876	8.347				0.102	35.325												
93.440	-171.740	1.0703549	1.179511	114.771	26.397	8.205		0.098	34.700	114.639	26.367	8.191				0.100	34.658												
99.451	-77.636	0.571629	1.026519	99.885	22.973	4.156		0.057	27.186	99.785	22.951	4.150				0.052	27.153												
105.825	-78.325	0.512634	0.512634	99.765	23.179	4.186	17.164	+0.057	27.221	99.605	22.951	4.179	27.134	+0.052	27.156	+0.052	27.156												
116	—	—	—	—	97.304	22.380	—	—	22.380	97.210	22.358	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	
125	—	—	—	—	100000	22.380	—	—	22.380	97.210	22.358	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	
133.193	60.043	0.330262	1.012176	92.594	22.446	-3.612	0.044	18.878	96.647	22.229	-3.614	0.043	18.658																
—	—	55.676	—	1.0202971	99.574	22.442	-4.13	19.629	97.073	22.478	-3.612	0.043	19.607	10.043	14.172														
—	60	—	—	1.0202976	97.594	22.447	-3.609	18.882	96.647	22.229	-3.611	—	18.661																
$(b) = T_c R_o (R_o / R_T)$																													

Calibration Data Sheet

Calibration Data Sheet

Calibration Data Sheet

Calibration Data Sheet

CALIBRATION DATA SHEET											
SN 19 N.C. Chamber											
Temp.	Inverse 100/K of 100/K 100/K	Element $E_0 = 96.8696$	No. LOAD	Element Current Output Temperature C	Element Current Output Temperature K	Reg. mv	Reg. mv	Reg. mv	Reg. mv	Reg. mv	Reg. mv
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)
16.346	-253.804	5.169227	2.287164	221.558	9.703	0.316	60.977	221.067	50.845	9.680	0.307
20.150	-25.53	4.612280	2.123034	216.058	119.63	9.696	59.705	215.592	49.586	9.673	59.566
23.156	-24.994	431.8535	2.053047	198.879	45.742	9.68	55.726	198.484	45.651	9.646	55.604
L-N2	27.070	-24.080	3.694227	1.881448	182.517	41.929	9.627	51.722	182.184	41.902	9.604
L-N2	27.175	-24.011	3.686173	1.867122	182.282	41.925	9.626	51.551	181.951	41.899	9.603
31.360	-21.710	3.188776	1.753669	169.874	39.071	9.575	6.301	48.947	169.586	39.005	9.553
38.882	-23.4248	2.591884	1.592913	154.305	35.190	9.476	0.277	45.243	154.068	35.436	9.455
48.076	-23.5074	2.080239	1.464353	141.852	32.626	9.323	0.247	42.196	141.651	32.560	9.304
63.806	-20.9344	1.587257	1.324726	128.333	29.516	8.998	0.195	38.709	128.169	29.479	8.932
L-N2	71.474	-195.676	1.290251	1.246116	120.711	22.763	8.660	0.153	36.576	120.565	22.530
L-N2	71.48	-195.731	1.291689	1.246383	120.737	22.769	8.662	0.153	36.584	120.571	22.536
B2.550	-190	1.202645	1.21196	118.297	21.208	8.595	0.147	35.860	118.158	21.196	8.491
B2.561	-184.589	1.129165	1.200913	116.284	21.745	8.350	1.141	35.236	116.149	21.714	8.336
C2.550	-179.720	1.070778	1.17724	114.037	21.228	8.206	0.136	34.570	113.907	21.199	8.192
C2.554	-172.696	0.511629	1.025684	9.9356	22.652	4.156	0.029	22.037	9.9258	22.829	4.150
G2	174.534	-78.116	0.515160	0.325968	99.386	21.859	4.192	27.058	+0.029	27.087	99.278
Iee	—	—	—	—	96.870	21.280	—	—	22.280	96.776	21.258
ICe	—	—	—	—	91.870	21.280	—	—	21.280	91.776	21.258
333.192	60.043	0.300126	1.002129	97.125	21.339	3.612	0.002	18.729	97.031	21.317	-3.614
—	60.442	—	1.602646	97.126	21.339	3.617	0.702	+0.002	16.704	97.032	21.317
—	60	—	1.002627	97.114	21.339	3.609	—	—	18.730	97.129	21.317
$(6) = I_C e_0 (R_1 / R_0)$											
22.280008											
$\text{Transducer Calibration Data}$											
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CALIBRATION DATA SHEET

SN 22

4/10/66
P April 1966

Temp.	Invar Temp. 100/K by 100	No LOAD						100 K LOAD					
		K	C	Element $R_o = 98.7696$	TC R_T	Transducer Output	Correlation Object	Element	TC	Transducer Output	Correlation Object	Connected Transducer	Connected Output
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)
19.295	-253.855	51.024680	2.339274	23.050	53.141	9.704	-0.020	62.825	230.518	53.019	9.681	-0.035	62.665
26.150	-253.3	4.962780	2.275286	224.730	51.668	9.696	61.364	224.225	51.572	9.673	61.210		
20.871	-252.279	4.761338	2.225398	219.803	51.204	9.690	60.874	219.320	50.444	9.667	60.076		
23.290	-249.660	4.295331	2.087104	206.222	47.431	9.667	57.078	205.798	47.334	9.645	52.944		
26.471	-246.479	3.772464	1.943389	191.949	44.128	9.633	53.791	191.581	44.064	9.610	53.639		
LN-27.329	246.011	3.682924	1.911040	189.445	42.572	9.626	-0.020	53.178	189.088	42.490	9.603	53.093	-0.035
30.956	-242.164	3.20440	1.795708	177.362	40.793	9.580	-0.015	50.358	177.049	40.721	9.558	-0.029	50.250
37.784	-235.346	2.644911	1.639707	161.954	37.249	9.491	-0.006	46.734	161.692	37.189	9.470	-0.018	46.641
42.124	-231.672	2.373530	1.565463	154.635	35.586	9.438	45.004	154.396	35.511	9.417	-0.013	44.915	
LN-42.514	-195.631	1.290001	1.260542	124.504	28.636	6.659	0.089	37.344	124.389	28.609	8.644	+0.043	37.296
LN-46.774	-195.724	1.291556	1.266980	124.547	28.646	8.662	37.302	124.352	124.392	28.610	8.647	37.257	+0.043
LN-51.150	-193.0	1.222645	1.235927	122.703	28.222	8.505	+0.044	36.771	122.552	28.167	8.491	+0.038	36.716
LN-54.689	-78.961	0.513637	1.030223	101.755	23.404	4.192	-0.042	27.554	101.651	23.380	4.185	-0.048	27.517
CO-59.532	-78.618	0.514960	1.030480	101.758	23.404	4.193	-0.042	27.561	101.654	23.380	4.182	-0.048	27.524
LN-65.0	—	—	—	1.00000	98.770	22.717	—	27.717	98.672	22.695	—	-0.006	22.689
LN-66.0	—	—	—	1.00000	98.770	22.717	—	22.717	98.672	22.695	—	-0.006	22.659
AMR-29.5440	22.290	0.338070	0.99986	98.670	22.694	-1.208	-0.038	21.388	98.572	22.672	-1.207	0.004	21.379
—	60.457	—	1.010528	98.921	22.752	-2.628	19.114	+0.020	19.134	98.823	22.729	-3.640	19.089
—	58.240	0.301759	1.0013380	98.906	22.748	-3.498	—	19.270	98.808	22.726	-3.500	0.020	19.246
—	60	—	1.001497	98.918	22.751	-3.609	—	19.162	98.820	22.729	-3.611	0.021	19.139
			23.7770				(6) - $T_L L_0 (A\%k)$						

CALIBRATION DATA SHEET

SN 23

Temp.	Invertor 100/K or 100/ 100/	Element $R_0 = 98.5435$				No Load				100K LOAD						
		K	C	RT/R ₀	RT	mv	mv	mv	mv	mv	mv	mv	mv			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)			
19.295	-253.055	5.182480	2.345606	231.115	53.163	9.704	-0.728	62.139	230.582	53.034	9.681	-0.739	61.976			
20.150	-253.2	4.942274	2.281091	224.689	51.678	9.696		60.646	224.185	51.563	9.673		60.497			
20.871	-253.279	4.791138	2.266024	219.655	50.521	9.690		59.483	219.173	50.410	9.667		59.338			
23.280	249.860	4.292631	2.091057	206.059	47.394	9.667		56.333	205.635	47.296	9.645		56.202			
26.471	246.679	3.772461	1.944625	191.790	44.112	9.633		53.017	191.422	44.027	9.610		52.898			
L Ne	27.134	-246.916	3.6685143	1.921265	48.322	43.544	9.624	53.170	52.442	188.965	43.462	9.603	-0.739	52.324		
30.950	-242.194	3.230470	1.777675	177.150	40.744	9.580	-0.710	49.614	176.837	40.673	9.558	-0.730	49.501			
37.784	-235.366	2.6449111	1.641638	161.773	37.208	9.491	-0.672	46.927	161.511	37.148	9.470	-0.693	45.925			
42.124	-231.676	2.373930	1.567412	154.458	35.525	9.438	-0.668	44.295	154.220	35.471	9.417	-0.676	44.212			
L N ₂	77.519	-195.631	1.290001	1.260766	124.241	28.575	8.657	-0.514	36.720	124.087	28.540	8.644	-0.524	36.640		
L H ₂	77.426	-195.724	1.291656	1.261208	124.241	28.565	8.662	37.247	-0.514	36.733	124.130	28.557	37.197	-0.524	36.623	
C O ₂	63.150	-150	1.202645	1.262690	123.465	28.374	8.505	-0.507	36.372	123.313	28.362	8.491	-0.516	36.337		
C C ₂	144.689	-26.461	0.513639	1.020263	101.531	23.352	4.192	-0.367	27.177	101.498	23.328	4.185	-0.370	27.143		
C C ₂	194.725	-28.365	0.513900	1.030286	101.528	23.351	4.186	27.527	-0.367	27.172	101.425	23.328	4.181	27.509	-0.370	27.139
I _{EE}	—	—	—	—	98.544	2.2665	—	—	22.665	98.447	22.643	—	-0.008	22.635		
I _{CC}	—	—	—	—	1.000000	2.2665	—	22.665	—	92.665	22.643	—	-0.008	22.635		
A _{EE}	—	—	—	—	0.300000	98.544	2.2665	—	92.665	22.643	—	-0.008	22.635			
A _{EE}	295.440	22.290	0.3388779	0.9799752	96.568	22.211	-1.298	-0.139	20.774	96.474	22.189	-1.297	-0.145	20.747		
—	—	56.301	—	1.000051	98.548	22.666	-3.377	19.259	-0.351	18.938	22.451	-3.376	19.246	-0.355	18.911	
33.390	58.240	0.300059	1.001197	98.662	22.692	-3.498	—	18.843	98.564	22.670	-3.500	—	18.815	—	18.727	
—	—	60	—	1.002337	98.764	22.716	-3.609	—	18.756	98.166	22.693	-3.611	—	18.727	—	18.727
(1)	=	$I_c R_o$	(R/k)	22.6650												

Kilobars
11 Band 1966

Calculated Full Range

Transducer Calibration Data

Transducer Calibration Data

Transducer Calibration Data

Calculated o Range

CALIBRATION DATA SHEET

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H.C. Chaudhury
111 April 1966

CALIBRATION DATA SHEET

SN 25

Temp.	Invertor Temp. 100°C or 100/ 100	No LOAD				100% LOAD										
		Element R ₀ = 99.1261	T _C	Thermal Conductivity 0.047	Element Thermal Conductivity 0.047	Element R ₀	T _C	Thermal Conductivity 0.047	Element R ₀							
(1)	K	C	R _{T/R₀}	R _T	mV	mV	R _T	mV	mV							
(1)	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)							
19.295	-253.855	51.182480	2.307186	228.911	52.647	9.704	-0.730	61.621	228.978	52.527	9.681	-0.736	61.4972			
21.150	-253	476.2780	5.248474	222.919	51.262	9.694	64.223	222.393	51.148	9.673	60.085					
20.871	-251.229	4.791338	2.201088	218.185	50.183	9.690	59.143	217.710	50.073	9.667	59.004					
23.290	-249.860	4.293631	2.072481	205.437	47.250	9.667	56.187	205.017	47.154	9.645	56.063					
24.471	-246.679	3.772461	1.933078	190.627	43.844	9.633	52.747	190.264	43.761	9.610	52.1635					
L1c	27.139	-244.011	3.683734	1.898351	187.155	43.052	7.626	52.679	-0.730	51.944	186.856	42.976	9.603	53.515	-0.736	51.837
50.950	-242.94	3.230440	1.779016	176.347	40.560	9.580	-0.726	49.944	176.037	40.489	9.558	-0.732	49.315			
37.784	-235.364	2.649111	1.627166	161.295	37.098	9.491	-1.719	45.870	161.036	37.038	9.470	-0.726	45.782			
42.124	-231.676	2.371920	1.555370	154.169	35.459	9.438	-0.717	44.180	153.932	35.404	9.417	-0.723	44.098			
L1d	77.519	-195.631	1.290001	1.251344	124.537	28.644	8.659	-0.687	36.616	124.382	28.608	8.644	-0.695	36.557		
L1e	77.471	-195.679	1.270186	1.251571	124.551	28.617	8.665	37.304	-0.687	36.622	124.402	28.617	8.645	-0.695	36.563	
(2)	83.150	-190	1.202656	1.222258	127.149	2.6 C9.4	8.505	-0.678	35.921	122.000	2.6 E6.0	8.491	-0.685	35.866		
CB	194.689	-78.461	0.513039	0.28999	102.000	2.3460	9.192	-0.504	27.148	101.896	23.936	4.185	-0.508	27.113		
CC	194.532	-78.616	0.514000	1.290494	122.664	23.342	4.189	27.160	-0.704	27.156	101.902	23.427	4.174	27.124		
EE	—	—	—	1.000000	99.126	22.799	—	—	22.799	99.028	22.776	—	—	—	-0.017	22.759
EE	—	—	—	1.000000	99.114	22.797	—	22.797	99.025	22.774	—	—	—	-0.017	22.759	
AA	295.440	2.290	0.338477	0.999461	99.023	22.787	-1.298	-0.158	21.331	98.975	22.764	-1.297	-0.170	21.297		
BB	—	5.933	—	1.000289	99.204	22.817	-3.417	19.400	-0.404	18.996	99.106	22.791	-3.415	-0.407	18.971	
CC	331.490	58.340	0.391668	1.000843	98.209	22.818	-3.567	19.103	10.405	18.847	99.111	22.796	-3.569	19.075	18.820	
CC	—	60	—	1.013917	101.306	23.116	-3.609	—	—	23.093	100.405	23.093	-3.611	—	—	
$(6) = I_C L_0 (k/r_0)$																

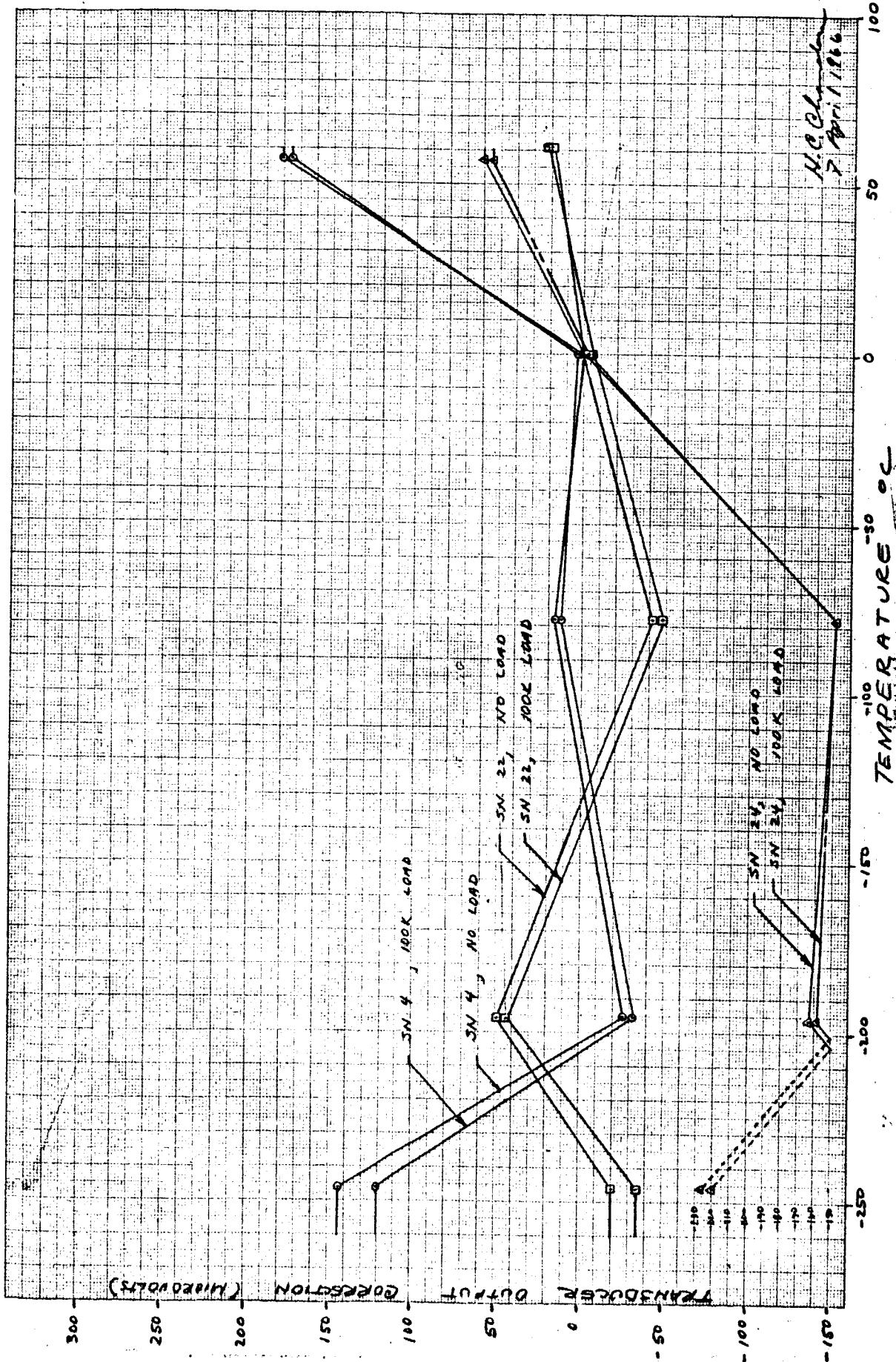
Calibration Data
12 April 1966

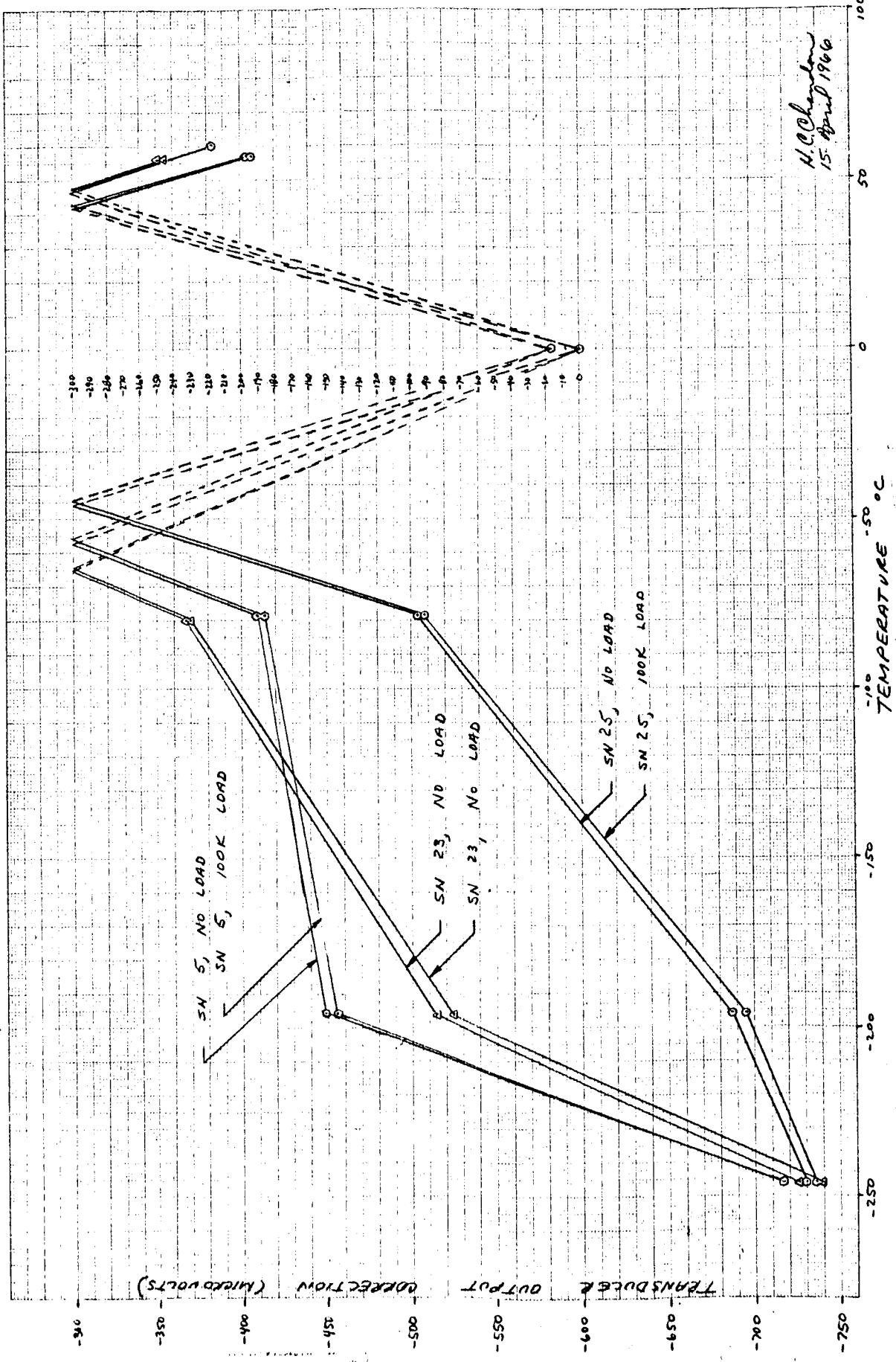
Calculated Full Range

Transistor Calibration Data

Enclosure 10
0700:1161

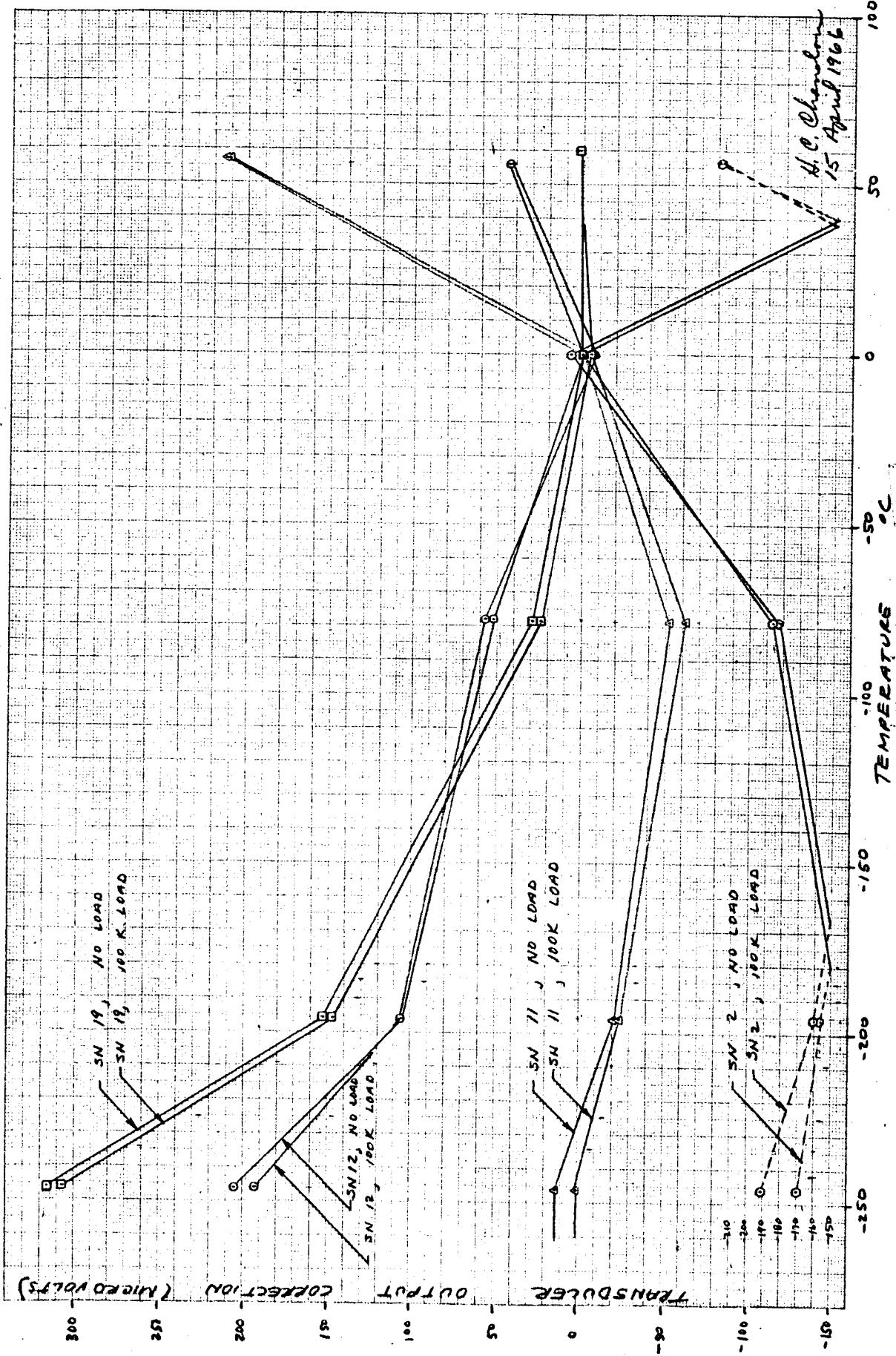
**TRANSDUCER OUTPUT CORRECTION
CURVES FOR 13 PRODUCTION TRANSDUCERS**

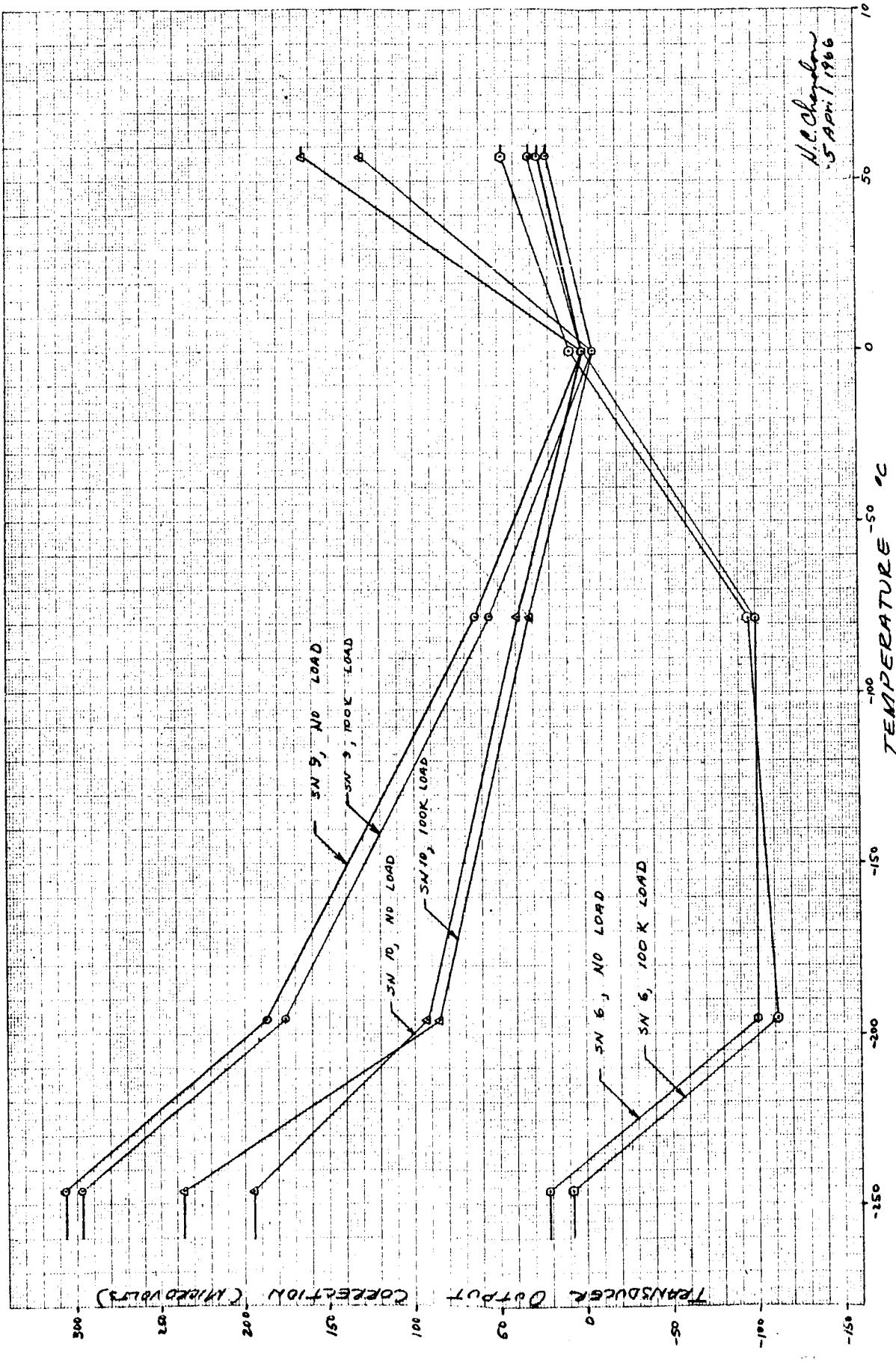




H.C. Chelton
15 April 1966

TEMPERATURE °C

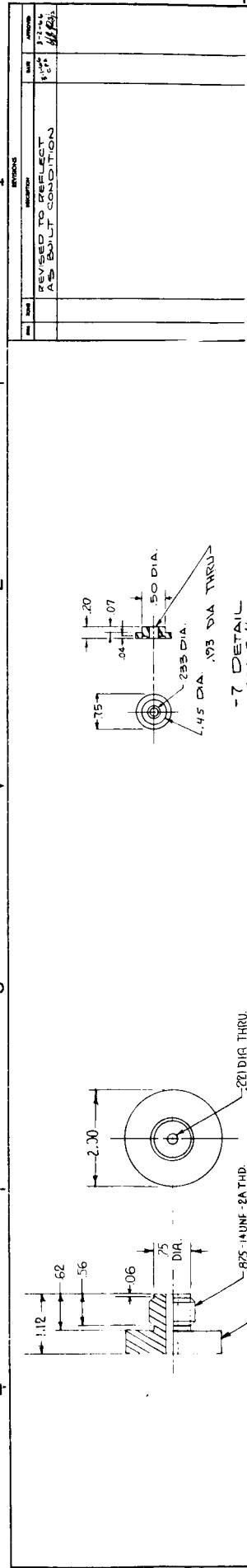




Enclosure 11
0700:1161

FABRICATION DRAWINGS

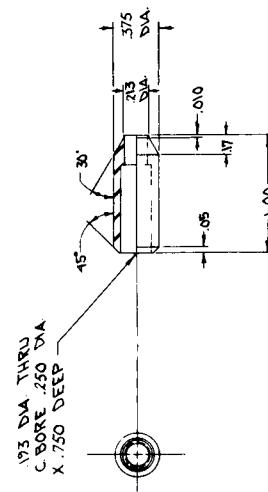
FOR MODEL RJ-100 THERMOCOUPLE REFERENCE JUNCTION



△ ACCEPTANCE TEST PROCEDURE

STEP 1. THE RESISTANCE BETWEEN THE TERMINALS ON THE WIRES SHALL NOT EXCEED THE VALUES SPECIFIED BELOW (MEASURED AT AMBIENT TEMPERATURE $72 \pm 5^\circ\text{F}$)

RED TO BLUE - 6 OHMS
TAN TO BLACK - 9 OHMS
TAN TO TAN (THE INSULATION RESISTANCE BETWEEN EACH PAIR OF WIRES (RED, BLUE AND TAN BLACK) SHALL BE GREATER THAN 10,000 MEGA OHMS AT AN AMBIENT TEMPERATURE $72 \pm 5^\circ\text{F}$. WIRES FEED WITH 50 VOLTS AC, BRIGHT THERMOCOUPLE, 100 FT. LEAD)



NOTE: ALL PARTS SHALL HAVE A $\frac{1}{16}$ OR BETTER.

ITEM NO.	PART NO.	DESCRIPTION	QUANTITY	UNIT	SPECIFICATION		DRAWING NO.
					MIN.	MAX.	
UNLESS OTHERWISE SPECIFIED							
1	05824-D	REFERENCE JUNCTION, THERMOCOUPLE MODEL RJ-100	1	PCB	DO NOT SCALE DRAWING	DO NOT SCALE DRAWING	1125448
2							